STATE OF VERMONT AGENCY OF TRANSPORTATION

Scoping Report

FOR

Springfield IM 091-1(83) I-91 Bridges 28 N&S over US Route 5

August 25, 2020



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I. Site Information

Bridges 28 N&S are located along Interstate 91 (I-91) at the interchange of exit 7 at mile marker 41.6 and cross over US Route 5 in the Town of Springfield. The existing conditions were gathered from a combination of a Site Visit, the Inspection Report, the Route Log and Orthophotos. See correspondence in the Appendix for more detailed information.

Roadway Classification	I-91: Principal Arterial – Interstate, National Highway System
	US Route 5: Major Collector
Bridge Type	28N: 4 Span Rolled Beam
	28S: 4 Span Rolled Beam
Bridge Lengths	28N: 202-feet
	28S: 207-feet
Year Built	1965
Ownership	State of Vermont

Need

Bridges 28 N&S carry Interstate 91 over US Route 5. The following is a list of deficiencies of Bridges 28 N&S in this location:

- 1. While the deck on bridges 28N and 28S are rated as fair and satisfactory respectively, they have minor maintenance needs as follows:
 - *Wearing surface:* There are patched areas in the pavement surrounding the joints along with some depressions and minor cracking. Potholes are likely to form in the near future.
 - *Curbs:* The curbs are concrete with granite facing. The concrete areas of the curbs have large areas of spalling with deep voids, scaling, and exposed reinforcing. The curb ends surrounding the bridge joints have large spalled-out openings that allow runoff to fall onto the substructures and beam ends below.
 - *Joints:* The Replacement fabric troughs have moderate debris build up. Additionally, the finger plate joints have some minor rust staining.
 - *Fascia:* The bridge fascias are in fair condition, with scattered areas of spalling with scaling and exposed reinforcing due to the spalled-out joint ends and curbs.
 - *Reinforced concrete deck:* The deck has patched areas scattered throughout and transverse cracks with minor saturation and small delaminations.
- 2. While the superstructure on bridges 28N and 28S are rated as fair and satisfactory respectively, they have minor maintenance needs as follows:
 - *Lateral Bracing:* The channel diaphragms are in good to satisfactory condition. The diaphragms over the middle pier and abutments have rust scale with minor to moderate pitting/section loss, due to the saturation of the surrounding area of the joints.
 - *Rolled Beams:* The beams have scattered paint peel with exposed primer and some minor rust scale, mostly along the fascia beams. The beam ends at the abutments and pier 2 have rust scale with minor to moderate section loss, mostly along the west fascia.

- *Bearings:* The pedestal bearings have areas of rust scale with minor to moderate section loss at the abutments and at pier 2. Some of the swedge bolts in the west ends have significant section loss.
- 3. While the substructure on bridges 28N and 28S are rated as fair and satisfactory respectively, they have minor maintenance needs as follows:
 - *Reinforced concrete backwalls:* The backwalls have large areas of saturation with map cracking and scattered rust staining. Additionally, there are areas of minor spalling in the west ends.
 - *Abutment 1 and 2 seat/stem:* The abutments are in satisfactory condition with some minor to moderate distress. There are scattered areas with saturation, map cracking, and small areas of rust staining.
 - *Wingwalls:* The wingwalls have some map cracking with light staining.
 - *Piers seat/caps:* The caps of piers 1 and 3 are in good condition. The cap of pier 2 has fine map cracks in the ends and some scattered delaminations. The west end has moderate saturation and some scattered small areas of rust staining.
 - *Pier columns:* The pier columns are in fair condition with moderate distress. The columns of piers 1 and 3 are in good condition while the west column of pier 2 has vertical cracking with delaminations and spalling in the base with exposed reinforcing.

Traffic

A traffic study of this site was performed by the Vermont Agency of Transportation. The traffic volumes are projected for the years 2024 and 2044.

Section	AADT		DHV		%T		%D		ADTT		ESALs	
Section	2024	2044	2024	2044	2024	2044	2024	2044	2024	2044	(2024~2044)	(2024~2044)
1	8,600	9,400	1,400	1,600	13.8	20.1	100	100	1,500	2,400	10,392,000	23,970,000
2	4,200	4,700) 860 960		13.9	20.3	100	100	830	1,400	5,651,000	13,133,000

Section 1 – Bridge 28 Northbound Section 2 – Bridge 28 Southbound

The 2018 AADT on US Route 5 under Bridges 28 N&S is 3,470 vehicles per day.

Design Criteria

The design standards for this project are the Vermont State Standards (VSS), dated October 22, 1997, A Policy on Geometric Design of Highways and Streets (Green Book), 7th Edition, the VTrans Structures Design Manual, dated 2018, and Interstate Scoping Guidance, dated 2014. Minimum standards are based on the traffic volumes listed above and a design speed of 70 mph.

Design Criteria	Source	Existing Condition	Minimum Standard	Comment
Approach Lane and Shoulder Widths	Green Book Chapter 8.2	4'-12'-12'-10' (38')	4'-12'-12'-10' (38')	
Bridge Lane and Shoulder Widths	Green Book Chapter 8.2	NB: 3'-12'-12'-3' (42') SB: 3'-12'-12'-3' (30')	NB: 4'-12'-12'-10' (50') SB: 4'-12'-12'-10' (38')	Substandard shoulder widths both northbound and southbound
Clear Zone Distance	VSS Table 3.4	Clear or Shielded	26' fill / 20' cut	
Banking	VSS Section 3.13	NB: 5.6% SB: 8%	8% (max)	Northbound slightly substandard
Speed		65 mph (Posted)	70 mph (Design)	
Horizontal Alignment	AASHTO Green Book Table 3-10b	$\frac{R_{\text{NORTHBOUND}} = 2,865}{R_{\text{SOUTHBOUND}} = 1,910}$	$\begin{array}{c} R_{min} = 2,790" @ 6.6\% \\ R_{min} = 1,810" @ 8\% \end{array}$	Northbound slightly substandard
Vertical Grade	AASHTO Green Book Table 8-1	NB: -2.71% (max) SB: -1.01% max)	4% (max) for rolling terrain	
K Values for Vertical Curves	AASHTO Green Book Table 3-35	$\begin{array}{l} K_{CREST-NB} = 210 \\ K_{CREST-SB} = 312 \end{array}$	247 crest / 181 sag	Northbound slightly substandard
Vertical Clearance Issues	VSS Section 5.8	14'-11" (below 28N) 17'-4" (below 28S)	14'-3" (min)	
Stopping Sight Distance	AASHTO Green Book Table 3-35	NB: 673' SB: 821'	730'	Northbound slightly substandard
Bicycle/Pedestrian Criteria		None	N/A	Limited Access
Bridge Railing (and Approach Railing)	Structures Design Manual Section 13.2	2-rail curb mounted box beam	TL-5	Substandard
Structural Capacity Structures Design Manual Section 3.4.1		Structurally Sufficient (28N&S)	Design Live Load: HL-93	

Inspection Report Summary

Bridge	Deck Rating	Superstructure Rating	Substructure Rating	Channel Rating
28 N	5	5	5	N/A
28 S	6	6	6	N/A

Bridge 28 N:

5/17/2018 – This structure should be considered for a deck replacement project, eliminating the joint over pier 2 and new joints installed over the abutments. Concrete repairs are needed to pier 2 and abutment 2, removing all loose concrete and delams. The west fascia beam ends over pier 2 need to have steel repairs made. New bearings should be set in areas below the joints, mostly along the west fascia. ~JW/MC

5/16/2016 – This structure needs to have concrete repairs to the curbs with new seals installed especially in the ends surrounding the joints. The finger plate joints should be considered for replacement with Vermont joints and should extended to the fascias with scuppers installed.

Concrete repairs are needed to abutment 2, piers 2 and 3 with all loose concrete/delams removed and then patched. ~JW/AC

5/15/2014 – Curbs need major repair soon. Weep tubes should be extended below the beams. Bearing have been greased however the heavy rusting should have been cleaned. the bearing on abutment #1 side under beam #1 and #5 should be cleaned and reset as bearing #5 on abut#1 could fail. Erosion in the slopes at the drain troughs should be repaired. Beams should be spot cleaned and painted. ~FRE/TJB

5/22/2012 - Curbs should be cleaned and patched along with the columns on pier #3. ~FRE/SJH

Bridge 28 S:

5/18/2018 – This structure should be considered for a deck replacement project, or new fascias installed to replace the heavily deteriorated cubs and affected soffit below. New joints over the abutments should be installed as well. The beams need general cleaning and painting. ~JW/MC

5/16/2016 – This structure needs to have concrete repairs to the curbs with new seals installed especially in the ends surrounding the joints. The finger plate joints should be considered for replacement with Vermont joints and should extended to the fascias with scuppers installed. \sim JW/AC

5/15/2014-Curbs should be cleaned of all loose material and patched. Beams should be spot cleaned and painted. ${\sim}FRE/TJB$

5/22/2012 – Curbs should be cleaned and patched along with the spalling in the fascias. ~FRE/SJH

04/12/2010 – Left top rail near abutment No.2 needs repair or replacement. Column No.1 of pier No.2 needs repair. The curb areas on both sides are in need of repairs. ~PLB

Hydraulics

Bridge 28 N&S is a dry crossing, so hydraulics is not applicable.

Utilities

Aerial Utilities:

- There are no known aerial utilities within the project limits.
- Approximately 615 feet to the south of the bridges there is an aerial crossing for a power service. These should not be impacted by the project. FirstLight has buried fiber in bike path/Toonerville Trail approximately 660 feet south of bridges. It is not expected that this will be impacted by the project.

Underground Utilities:

• There are no known underground utilities within the project limits.

Municipal Utilities:

• No known water or sewer lines exist within the project limits.

Right of Way

The existing approximate Right-of-Way is shown on the Existing Conditions Layout sheet.

It is anticipated that Right-of-Way acquisitions will not be required for any work associated with this project.

Resources

The resources present at this project are shown on the Existing Condition Layout sheets.

Archaeological:

There are no archaeologically sensitive areas within the project area.

Historic:

The project is considered EXEMPT for above-ground historic resources per the Section 106 Exemption Regarding Effects to the Interstate Highway System adopted by the Advisory Council on Historic Preservation on March 10, 2005.

Natural Resources:

Wetlands/Watercourses

There are no wetlands or watercourses within the review area.

Wildlife Habitat

There is very limited wildlife habitat at this location.

Rare, Threatened and Endangered Species

The only listed species in the project area is the federally threatened northern long-eared bat. The bridge does not provide useful roosting habitat, so restrictions caused by this animal are unlikely.

Agricultural Soils

There are no mapped agricultural soils in the review area.

Hazardous Materials:

There are no hazardous waste sites located in the immediate vicinity of the bridge. The hazardous waste sites located in the project area are shown on the map to the right. There are several hazardous waste sites in close proximity to the project area.

Stormwater: No known issues.

II. Safety

Crashes from the last 5-year period are shown to the right. Each black dot on the map represents a crash.

Interstate 91: There have been 9 crashes located in the project area along Interstate 91 in Springfield within the last 5-year period.

US Route 5: There have been 19 crashes located along US Route 5 and at the I-91 ramps at exit 7 in Springfield within the last 5-year period.

The following High Crash Locations are located within the project area:

High Crash Location Segment:

Route	Town	Mileage	# of Crashes	# of Fatalities	# of Injuries
I-91	Springfield	41.5 - 41.8	11	0	2

The VTrans Traffic Safety Engineer evaluated the project site with the following findings:

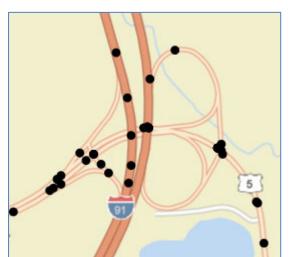
High Crash Segment, I-91, MM 41.5 - 41.8

This section of I-91 includes Bridges 28 N & S as well as the I-91 NB on ramp and the I-91 SB on ramp at exit 7.

Crashes from 2010 and up were reviewed by the VTrans Highway Safety Engineer with the following findings:

"The project area was identified as a high crash location between mile points 41.5 and 41.8 in the 2010-2014 HCL report. The project was not identified as a high crash location in subsequent HCL reports (2012-2016 and draft 2014-2018).

A review of crashes since 2010 indicates that most of the crashes happened in the southbound direction (a collision diagram is attached for reference).





From the data available, it appears that the area of the bridge, in the southbound direction, is prone or was prone to black ice and being slippery. The following two statements from crash narratives from two different years are indicative of this: "Interstate 91 was clear and dry in either direction about a mile from the scene"; "The bridge in this area had more slush ice than other areas on the interstate".

I followed up with the District to see if they had more information about this issue. The District indicated that the bridge has had inherent joint issues and that the plows have to be raised a little so they do not catch the steel joint. They indicated that this tends to leave some residue on the bridge deck at times which could cause ice and did mention that they put salt to all of the bridges at a higher rate.

Because there are several crashes listed at mile point 41 that do not have information (since they are considered non-reportable) but that may well have happened in the area of the bridge, we contacted the VSP Westminster barracks to obtain more details. While some of the more recent "non-reportable" crashes have involved vehicles that slide off, the data is inconclusive as to whether these happened at the bridge.

Based on the above discussion, there has been an issue with the bridge icing (potentially because of issues with the steel joint and the need for the plows to be lifted slightly), and this caused crashes in the past. It is not clear if this type of crash is still happening. The District mentioned that they are putting more salt on the bridges. In light of this, I do not have any suggestions to reduce the frequency of crashes."

III. Maintenance of Traffic

The Vermont Agency of Transportation reviews each new project to determine suitability for the Accelerated Bridge Program, which focuses on faster delivery of construction plans, permitting, and Right of Way, as well as faster construction of projects in the field. One practice that will help in this endeavor is closing bridges for portions of the construction period, rather than providing temporary bridges. In addition to saving money, the intention is to minimize the closure period with faster construction techniques and incentives to contractors to complete projects sooner. The Agency will consider the closure option on most projects where rapid reconstruction or rehabilitation is feasible. The use of prefabricated elements in new bridges will also expedite construction schedules. This can apply to decks, superstructures, and substructures. Accelerated Construction should provide enhanced safety for the workers and the travelling public while maintaining project quality. The following options have been considered:

Option 1: Off-Site Detour

This option would close the section of I-91 between the on and off ramps at exit 7.

I-91 Northbound: Traffic traveling northbound on I-91, would utilize US Route 5 between exit 6 and exit 8. The through distance on the US Route 5 detour is almost identical at 20.8 miles versus the 17.7 miles on I-91, with travel times estimated at 28 minutes for the detour route and 19 minutes for traveling on I-91.

I-91 Southbound: The detour would utilize the on and off ramps at exit 7 for southbound traffic. This detour would not add any distance to the through route. The median between US Route 5 northbound and southbound currently restricts traffic from traveling straight across and would need to be modified to allow traffic to cross over US Route 5 during construction.

It is recommended that a detour only be utilized for brief closure periods during off peak hours, such as nights or weekends, in order to rapidly replace the deck or superstructures. The methods available to replace a deck or superstructure during a short closure period include: lateral slide, self-propelled modular transporters (SPMTs), and prefabricated bridge elements. Each of these methods is discussed briefly below.

Lateral Slide

lateral slide consists А of constructing an entire superstructure adjacent to the location where it is intended and physically pushing or pulling the structure into its design location along lubricated rails. This allows traffic to be maintained on the existing bridges while construction of the bridges takes Traffic would then be place. detoured for approximately 3 days while the existing bridge is removed and the new bridge is moved into place.



[Images from "Accelerated Bridge Construction - Experience in Design, Fabrication and Erection of Prefabricated Bridge Elements and Systems" from FHWA (2011).]

One of the disadvantages of utilizing a lateral slide for Bridges 28 N&S is that the construction still needs to take place over US Route 5. There are some height restrictions and worker safety issues when construction occurs over busy roadways.

Self-Propelled Modular Transporters (SPMT)

There are several methods of constructing the bridge in a less restricted safer. environment before moving it into place. One of those methods utilizes SPMTs. Similar to a lateral slide, SPMT placement requires that the entire superstructure is constructed near but not in its intended location, allowing traffic to be maintained on the existing bridges while the new



bridges are constructed. Instead of sliding the superstructure into place, it is lifted off its temporary blocking, moved a short distance to its design location, and lowered into place. This method can also be used in reverse to remove the existing superstructure.

Superstructures have been removed and replaced utilizing SPMTs during 12 hour stretches overnight. This type of technology has been used in several states, including Florida, Louisiana, Minnesota, Rhode Island, New York, Illinois, Washington, and Utah. It is reasonable to assume that the I-91 closure period would be similar to that for a lateral slide to incorporate the site

preparation work, the cleanup and backfilling that may be required after the superstructure has been replaced. One of the disadvantages of using SPMTs is that US Route 5, in addition to I-91, needs to be closed to traffic while the move is taking place. While this is an additional inconvenience, it does not rule out the use of SPMTs because there are alternate methods for traffic to get to the other side of I-91 on US Route 5.

Prefabricated Bridge Units (PBU)

Another method of constructing the bridge in a safer and less restricted environment over US Route 5 is to prefabricate portions of the bridge structure and deliver those pieces to the construction site to be joined together to form the bridge. These bridge superstructure pieces are referred to as Prefabricated Bridge Units, or PBUs. Many substructure pieces can be prefabricated as well and lifted into place before the



PBUs are placed. Using rapid setting concrete for the joint closure pours, the closure period can be reduced to 3 days per bridge for this method of superstructure replacement as well.

Installation Costs

The baseline method of installing the superstructure is using a crane to lift the PBUs into place. These costs are included in the baseline bridge costs. The extra engineering and temporary supports required for a lateral slide are approximately \$150,000 per bridge, and the costs paid to an SPMT subcontractor would be around \$200,000 per bridge for a dry crossing.

A map of the detour route can be found in Appendix N.

Advantages: The costs associated with signing the detour are much lower than the construction costs associated with the other maintenance of traffic options. By detouring traffic away from construction activities, it creates a safer working environment for the construction workers. By not constructing the structure in phases, there will be no vibrations or deflections from adjacent traffic to affect the quality of the closure pours joining the phases. By not requiring the construction and removal of temporary approaches, temporary bridges and temporary crossovers, the length of construction can be reduced over those other options.

Disadvantages: Traffic will not be maintained along the existing corridor for a limited portion of construction. Through traffic will see an increase in travel times during the closure period.

Option 2: Temporary Bridges

The standard maintenance of traffic option based on the length of the bridges and the traffic volumes at these locations would be a one lane temporary bridge for each barrel of I-91. There is sufficient Right-of-Way located along this section of I-91 that a temporary bridge could be located east of the existing bridges while the northbound bridges are under construction and west of the existing bridges while the southbound bridges are under construction.

A one lane Mabey bridge is approximately 24' wide. The distance between the northbound and southbound bridges varies between 85' and 110'. Thus, it would seem that a temporary bridge could be launched between the north and south bound bridges to be utilized in turn for both the north and southbound traffic without being moved while work is being performed on each bridge.

This is the configuration shown in the Appendix and considered further in this report.

Advantages: A temporary bridge maintains traffic along the existing corridor during construction.

Disadvantages: There are extra costs associated with constructing or launching temporary bridges. Changes in traffic patterns can increase the probability of accidents and the increased time associated with constructing temporary approaches and launching the temporary bridges puts the construction workers at increased risk for accidents. In order to minimize the length of median affected by the temporary roadwork, the design speed should probably be reduced to more safely allow vehicles to navigate the temporary roadway. This decrease in speed would cause slight traffic delays.

Option 3: Phased Construction

Phased construction is the maintenance of one lane of traffic on the existing bridge while working on the other lane. The project begins with traffic being constricted to one lane, while work is done on the other. After completion of improvements to the first lane, traffic is switched to the completed lane and work proceeds on the second lane. Traffic flow is constant, although delayed due to slower speeds in the work zone. In the case of Interstate bridges, phasing is usually appropriate only for repairs or replacement of deck and/or railing. For bridge 28 N, the DHV volume of 1,400 vehicles per hour is slightly above the 1,250 vehicles per hour cutoff that guidance allows for one lane during peak hours, therefore phasing should be considered for a reasonable period of time without needing to reopen both lanes, but should be limited in order to reduce traffic congestion. For bridge 28 S, the DHV volume of 860 vehicles per hour is well below the 1,250 vehicles per hour cutoff that guidance allows for one lane during peak hours, therefore phasing could be considered for a reasonable period of time without needing to reopen both lanes. Periodic short-term lane closures or shifts on US Route 5 may be necessary to provide access to crews working on the superstructures from below. These shifts or closures would not be advised during peak hours.

Advantages: Traffic flow is maintained through the corridor during the project. Phasing the work allows the work to proceed one lane at a time without the expense of a temporary bridge or crossovers and without the inconvenience of a closure and detour.

Disadvantages: Compared to a closure and detour or a temporary bridge scenario, it takes longer and costs more to construct, rehabilitate, or repair a bridge project in phases because some of the construction tasks have to be performed multiple times and cannot be performed concurrently. Additional permit requirements may come into play. The safety risks for both workers and travelers are also increased due to the close proximity to each other. Some structural qualities, such as joints, demand more coordination time and may suffer in quality as well. Periodic lane closures outside of peak hours on US Route 5 may be required.

Option 4: On-Site Detour with Crossovers

Another method for maintaining traffic on parallel structures with multiple lanes of unidirectional traffic is creating a crossover in the median before and after the structures to get all traffic off one structure and on to the parallel structure. This option is rarely available for most projects, because

most non-interstate structures in Vermont do not have parallel bridges. The possibilities on interstates may even be limited based on site distance, traffic patterns or obstructions in the median.

Bridges 27 N&S over the Toonerville rail trail are located 600 feet south of Bridges 28 N&S. North of Bridges 28 N&S, the northbound and southbound barrels split from each other, with some large trees located in the median area. Additionally, the elevation of the northbound and southbound lanes have nearly a 10-foot difference between them just north of the bridges, requiring a large amount of fill for a crossover. While feasible, this makes the site not ideal for a crossover.

IV. Alternatives Discussion

While bridges 28 N&S are not structurally deficient there are major maintenance needs as described in the Needs section above.

Maintenance Schedule:

It is desired to keep the northbound and southbound direction for each bridge on the same maintenance cycle. Therefore, the recommended scope for Bridge 28N should be the same for Bridge 28S.

No Action

This alternative would involve leaving the bridges in their current condition. A good rule of thumb for the "No Action" alternative is to determine whether the existing bridge can stay in place without any work being performed on it during the next 10 years. While Bridges 28 N&S are in fair to satisfactory condition, there are maintenance issues that need to be addressed in order to extend the useful life of the structure and slow down the current deterioration. Since some work is required within the next 10 years, the No Action alternative will not be considered further in this report.

Alternative 1: Rehabilitation

This rehabilitation option includes the minimal amount of work necessary to extend the useful lives of the bridges. While the substructure, superstructure, and deck are rated as being in fair to satisfactory condition, there are maintenance issues that would need to be addressed with any rehabilitation. A rehabilitation for the bridges would include the following:

- Northbound substructure work: While piers 1 and 3 are in good condition, the middle pier has patched areas and significant cracking with large delaminations throughout. The superstructure should be shored at the middle pier, and new pier columns and a cap should be poured, or the existing pier should be encased in concrete. While the northern abutment is in satisfactory condition, the southern abutment has large areas of saturation with cracking and surrounding delaminations throughout. Additionally, there is a large area of spalling in the west end that is starting to undermine the bearing. Extensive concrete repairs or a new abutment stem should be poured.
- Southbound substructure work: While piers 1 and 3 are in good condition, the middle pier has patched areas and significant cracking with large delaminations throughout. The superstructure should be shored at the middle pier, and new pier columns and a cap should be poured, or the existing pier should be encased in concrete. There are scattered areas of fine cracking in the wingwalls and abutments. These areas should be prepared for concrete repair and repaired with the appropriate concrete class.

- The beams have some heavy rust scale with minor to heavy section loss, localized at the beam ends at the abutments and piers. The northbound bridge has a beam with a large hole in the web and has minimal section remaining in the flange, bending could soon occur. This beam should be repaired, and all other beams should be painted and repaired as needed.
- The concrete curbs behind the granite facing have a significant amount of map cracking with some heavily spalled areas with exposed reinforcing. The bridge fascias would be removed, and new fascias, curbing, and railing would be constructed.
- All exposed concrete on the bridges should be sprayed with silane water repellant. This should protect the degrading concrete for several years against moisture damage, at which point, a new application should occur.
- The existing decks would be membraned and paved.

The existing bridge components are in fair to satisfactory condition. It is reasonable to assume that with the repairs listed above, the existing substructure and beams can safely carry anticipated traffic loads for an additional 30 years.

The current curb to curb width of bridges 28N and 28S is approximately 42 feet and 30 feet wide respectively, which is substandard by 8-feet on each of the bridges. The overhangs may be increased slightly to provide a wider shoulder over the bridges. Any possible widening will be determined in design.

Advantages: This option provides the lowest upfront cost to extend the life of the structure.

Disadvantages: Having newer non-chloride laced concrete adjacent to the existing concrete usually exacerbates the rate of deterioration of the remaining concrete which surrounds the repairs. This can be mitigated for approximately 30 years with the addition of sacrificial anodes into the patched structure.

Maintenance of traffic: Most of this work can be accomplished with single lane closure utilizing phased construction on I-91. Individual lanes on US Route 5 may need to be closed as well while substructure and overhead repair work is occurring.

This alternative will address the deterioration issues of the existing bridges.

Alternative 2: Deck Replacement

A deck replacement for this bridge would include a new deck, curbs and railings, along with substructure concrete repairs. This option would include the following:

- The existing deck would be removed, and a new cast-in-place deck would be poured. The fascia detail would be modified to allow for a slightly wider structure. Along with the new decks, new backwalls would be poured and new bridge joints would be installed.
- Northbound substructure work: While piers 1 and 3 are in good condition, the middle pier has patched areas and significant cracking with large delaminations throughout. The superstructure should be shored at the middle pier, and new pier columns and a cap should be poured, or the existing pier should be encased in concrete. While the northern abutment

is in satisfactory condition, the southern abutment has large areas of saturation with cracking and surrounding delaminations throughout. Additionally, there is a large area of spalling in the west end that is starting to undermine the bearing. Extensive concrete repairs or a new abutment stem should be poured.

- Southbound substructure work: While piers 1 and 3 are in good condition, the middle pier has patched areas and significant cracking with large delaminations throughout. The superstructure should be shored at the middle pier, and new pier columns and a cap should be poured, or the existing pier should be encased in concrete. There are scattered areas of fine cracking in the wingwalls and abutments. These areas should be prepared for concrete repair and repaired with the appropriate concrete class.
- The beams have some heavy rust scale with minor to heavy section loss, localized at the beam ends at the abutments and piers. The northbound bridge has a beam with a large hole in the web and has minimal section remaining in the flange, bending could soon occur. This beam should be repaired, and all other beams should be painted and repaired as needed.
- The concrete curbs behind the granite facing have a significant amount of map cracking with some heavily spalled areas with exposed reinforcing. The bridge fascias would be removed, and new fascias, curbing, and railing would be constructed.
- All exposed concrete on the bridges should be sprayed with silane water repellant. This should protect the degrading concrete for several years against moisture damage, at which point, a new application should occur.
- The new decks would be membraned and paved.

The existing bridge components are in fair to satisfactory condition. It is reasonable to assume that with the repairs listed above, the existing substructure and beams can safely carry anticipated traffic loads for an additional 40 years.

The current curb to curb width of bridges 28N and 28S is approximately 42 feet and 30 feet wide respectively, which is substandard by 8-feet on each of the bridges. The overhangs may be increased slightly to provide a wider shoulder over the bridges. Any possible widening will be determined in design.

Advantages: This alternative would address the immediate concerns of the superstructure and substructure conditions and maintenance issues of the decks, with minimal upfront cost. The effects on the adjacent properties, resources, and wildlife would be minimal. The width of the existing bridges would be slightly widened.

Disadvantages: Having newer non-chloride laced concrete adjacent to the existing concrete usually exacerbates the rate of deterioration of the remaining concrete which surrounds the repairs.

Maintenance of Traffic: Traffic could be maintained on an offsite detour, a temporary bridge, crossovers or with phased construction.

Alternative 3: Superstructure Replacement

A superstructure replacement option for this bridge would include a new deck, railings, and beams, with substructure repairs as follows:

- The existing deck and beams would be removed, and new beams would be set, and a new cast-in-place deck would be poured. The fascia detail would be modified to allow for a slightly wider structure.
- The existing bridge seats would be cut down, and new bridge seats along with a new backwall would be poured to accommodate the new bearings and superstructure.
- Northbound substructure work: While piers 1 and 3 are in good condition, the middle pier has patched areas and significant cracking with large delaminations throughout. The superstructure should be shored at the middle pier, and new pier columns and a cap should be poured, or the existing pier should be encased in concrete. While the northern abutment is in satisfactory condition, the southern abutment has large areas of saturation with cracking and surrounding delaminations throughout. Additionally, there is a large area of spalling in the west end that is starting to undermine the bearing. Extensive concrete repairs or a new abutment stem should be poured.
- Southbound substructure work: While piers 1 and 3 are in good condition, the middle pier has patched areas and significant cracking with large delaminations throughout. The superstructure should be shored at the middle pier, and new pier columns and a cap should be poured, or the existing pier should be encased in concrete. There are scattered areas of fine cracking in the wingwalls and abutments. These areas should be prepared for concrete repair and repaired with the appropriate concrete class.
- All exposed concrete on the bridges should be sprayed with silane water repellant. This should protect the degrading concrete for several years against moisture damage, at which point, a new application should occur.
- The new decks would be membraned and paved.

The existing bridge components are in fair to satisfactory condition. It is reasonable to assume that with the repairs listed above, the existing substructure and beams can safely carry anticipated traffic loads for an additional 40 years.

The current curb to curb width of bridges 28N and 28S is approximately 42 feet and 30 feet wide respectively, which is substandard by 8-feet on each of the bridges. The overhangs may be increased slightly to provide a wider shoulder over the bridges. Any possible widening will be determined in design.

Advantages: This alternative would address the immediate concerns of the maintenance issues of the decks and beams, with minimal upfront cost. The effects on the adjacent properties, resources, and wildlife would be minimal. The width of the existing bridges would be slightly widened.

Disadvantages: Having newer non-chloride laced concrete adjacent to the existing concrete usually exacerbates the rate of deterioration of the remaining concrete which surrounds the repairs.

Maintenance of Traffic: Traffic could be maintained on an offsite detour while utilizing accelerated bridge construction techniques, a temporary bridge, crossovers or with phased construction.

Alternative 4: Complete Replacement

This alternative would replace the existing bridges with new superstructures as well as new substructures at the existing location. While the current horizontal alignment does not meet current standards for minimum radius and banking, this can be brought up to standard with modified banking. As such, an on-alignment option should be considered to reduce permanent impacts to adjacent properties and resources.

The various considerations under this option include: the bridge width and length, skew, superstructure type and substructure type.

a. Bridge Width

The current curb to curb width of bridges 28N and 28S is approximately 42 feet and 30 feet wide respectively, which is substandard by 8-feet on each of the bridges. Since a new 100-year bridge is being proposed, the bridge geometry should meet the minimum standards. As such, the standard typical section of 4'-12'-12'-10' (50' curb-to-curb) for the northbound bridge and typical section of 4'-12'-12'-10' (38' curb-to-curb) for the southbound bridge will be proposed.

b. Bridge Length and Skew

The existing bridges are each comprised of 4-spans totaling 202 and 207 feet-long with a skew of approximately 10 degrees and a maximum span of 55-feet. If a new steel beam bridge is proposed, the number of spans and span length could remain the same to allow for deep foundations similar to the existing configuration or be reduced down to two or one spans with taller abutments. The final bridge length will be determined in design.

c. Superstructure Type

The most economical superstructure type for this span is a steel girder superstructure with a cast-in-place composite concrete deck. If an offsite detour is chosen to be the preferred method of traffic control, then accelerated bridge construction methods would be recommended. These are explained in section III: Maintenance of Traffic of this report and could include a lateral slide, self-propelled Modular Transporters, or prefabricated elements. The most common type of prefabricated superstructure elements that can satisfy the anticipated span length are Prefabricated Precast Bridge Units (PBUs) or prefabricated precast deck slabs on steel beams.

The current vertical clearance over Bridge 28 N is 14'-11". This meets the minimum standard of 14'-3". However, it is recommended that the existing clearance does not decrease.

d. Substructure Type

The existing abutments and piers are founded on steel piles. The preliminary geotechnical report indicates that new abutments and piers could be founded on either spread footings bearing on suitable foundation soils, or deep foundations such as driven piles or drilled shafts extending to bedrock. Sufficient subsurface information should be obtained in design to verify the in-situ conditions and determine the best foundation type. The preliminary geotechnical report can be found in Appendix D.

Maintenance of Traffic: Traffic could be maintained on an offsite detour, a temporary bridge, crossovers or with phased construction.

V. Alternatives Summary

Based on the existing site conditions and bridge condition, there are several viable alternatives:

Bridges 28 North & South

Alternative 1a: Rehabilitation with Traffic Maintained on an Offsite Detour Alternative 1b: Rehabilitation with Traffic Maintained via Phased Construction Alternative 1c: Rehabilitation with Traffic Maintained on a Temporary Bridge Alternative 1d: Rehabilitation with Traffic Maintained on Crossovers Alternative 2a: Deck Replacement with an Offsite Detour Alternative 2b: Deck Replacement with Traffic Maintained via Phased Construction Alternative 2c: Deck Replacement utilizing a Temporary Bridge Alternative 2d: Deck Replacement with Traffic Maintained on Crossovers Alternative 3a: Superstructure Replacement with an Offsite Detour Alternative 3b: Superstructure Replacement with Traffic Maintained via Phased Construction Alternative 3c: Superstructure Replacement utilizing a Temporary Bridge Alternative 3d: Superstructure Replacement with Traffic Maintained on Crossovers Alternative 4a: Full Bridge Replacement with Traffic Maintained on an Offsite Detour Alternative 4b: Full Bridge Replacement with Traffic Maintained via Phasing Alternative 4c: Full Bridge Replacement with Traffic Maintained on a Temporary Bridge Alternative 4d: Full Bridge Replacement with Traffic Maintained on Crossovers

VI. Bridge 28 N&S Cost Matrix¹

			А	lternative 1:	Rehabilitatic	n	Alte	rnative 2: De	ck Replacem	ent	Alternat	ive 3: Superst	ructure Repl	acement	Alternative 4: Full Bridge Replacement				
Sp	ringfield IM 091-1(83)	Do Nothing	a. Offsite Detour	b. Phased Construction	c. Temporary Bridge	d. Crossovers	a. Offsite Detour	b. Phased Construction	c. Temporary Bridge	d. Crossovers	a. Offsite Detour	b. Phased Construction	c. Temporary Bridge	d. Crossovers	a. Offsite Detour	b. Phased Construction	c. Temporary Bridge	d. Crossovers	
	Bridge Cost	\$0	2,411,000	2,772,600	2,411,000	2,411,000	3,756,200	2,826,600	2,458,000	2,458,000	4,744,600	3,010,200	2,617,600	2,617,600	7,017,200	7,078,800	6,155,400	6,155,400	
	Removal of Structure	\$0	0	0	0	0	806,400	927,360	806,400	806,400	806,400	927,360	806,400	806,400	1,656,000	1,904,400	1,656,000	1,656,000	
	Roadway	\$0	62,000	90,000	62,000	62,000	538,000	606,000	422,000	422,000	488,000	632,000	440,000	440,000	642,000	848,000	590,000	590,000	
	Maintenance of Traffic	\$0	238,600	593,200	854,040	1,518,480	238,600	593,200	854,040	1,518,480	238,600	593,200	854,040	1,518,480	238,600	593,200	854,040	1,518,480	
	Construction Costs	\$0	2,711,600	3,455,800	3,327,040	3,991,480	5,339,200	4,953,160	4,540,440	5,204,880	6,277,600	5,162,760	4,718,040	5,382,480	9,553,800	10,424,400	9,255,440	9,919,880	
COST	Construction Engineering & Contingencies	\$0	677,900	691,160	665,408	798,296	800,880	742,974	681,066	780,732	941,640	774,414	707,706	807,372	1,624,146	2,084,880	1,851,088	2,479,970	
	Accelerated Premium	<u> </u>	077,500	0001,100	003,408	0	373,744	0	001,000	0	439,432	0	0	0	668,766	2,084,880	0	0	
	Total Construction	ŞU	0	0	0	0	373,744	0	0	0	439,432	0	0	0	008,700	0	0	0	
	Costs w CEC	\$0	3,389,500	4,146,960	3,992,448	4,789,776	6,513,824	5,696,134	5,221,506	5,985,612	7,658,672	5,937,174	5,425,746	6,189,852	11,846,712	12,509,280	11,106,528	12,399,850	
	Preliminary Engineering	\$0	542,320	691,160	499,056	798,296	533,920	495,316	454,044	520,488	941,640	774,414	707,706	807,372	1,433,070	1,563,660	1,851,088	1,983,976	
	Right of Way	\$0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Total Project Costs	\$0	3,931,820	4,838,120	4,491,504	5,588,072	7,047,744	6,191,450	5,675,550	6,506,100	8,600,312	6,711,588	6,133,452	6,997,224	13,279,782	14,072,940	12,957,616	14,383,826	
	Annualized Costs	\$0	131,061	161,271	149,717	186,269	176,194	154,786	141,889	162,653	172,006	134,232	122,669	139,944	132,798	140,729	129,576	143,838	
SCHEDULEING	Project Development Duration		3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	3 years	
	Construction Duration		6 months	9 months	2 years	2 years	9 months	2 years	2 years	2 years	9 months	2 years	2 years	2 years	2 years	2 years	3 years	3 years	
SCH	Closure Duration (If Applicable)		2 weeks each bridge	NA	NA	NA	4 weeks each bridge	NA	NA	NA	1 week each bridge	NA	NA	NA	2 weeks each bridge	NA	NA	NA	
	Typical Section - Roadway (feet)	38'	38'	38'	38'	38'	38'	38'	38'	38'	38'	38'	38'	38'	38'	38'	38'	38'	
	Typical Section - Bridge (feet)	NB: (42') SB: (30')	NB: 3'-12'-12'-3' (42') SB: 3'-12'-12'-3' (30')				NB: 3'-12'-12'-3' (42') SB: 3'-12'-12'-3' (30')			NB: 3'-12'-12'-3' (42') SB: 3'-12'-12'-3' (30')				NB: 4'-12'-12'-10' (50') SB: 4'-12'-12'-10' (38')					
BNI	Geometric Design Criteria	Substandard shoulder width	Substa	Substandard shoulder width on both bridges				Substandard shoulder width on both bridges				Substandard shoulder width on both bridges				Meets Minimum Standards			
ENGINEERING	Traffic Safety	Structurally Sufficient		Impro	oved		Improved			Improved				Improved					
DN G	Alignment Change	No Change		No Ch	ange			No Ch	ange			No Cł	nange		No Change				
	Bicycle Access	LAH		Limited Acce	ess Highway			Limited Acce	ss Highway			Limited Acc	ess Highway			Limited Acce	ess Highway		
	Pedestrian Access	LAH		Limited Acce	ess Highway			Limited Acce	ss Highway			Limited Acc	ess Highway		Limited Access Highway				
	US Route 5 Vertical Clearance	14'-11" (Minimum)		Meets Minimu	um Standards			Meets Minimu	ım Standards		Meets Minimum Standards					Meets Minimum Standards			
	Utilities	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	No Change	
	ROW Acquisition	No Change	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No	No	
OTHER	Road Closure	No	Yes	No	No	No	Yes	No	No	No	Yes	No	No	No	Yes	No	No	No	
	Design Life (years)	<10	30	30	30	30	40	40	40	40	50	50	50	50	100	100	100	100	

¹ Costs are estimates only, used for comparison purposes.

VII. Conclusion

Alternative 4c is recommended: a full bridge replacement while maintaining traffic on a temporary bridge during construction.

Discussion:

While all components of Bridges 28 N&S are rated in fair to satisfactory condition, both bridges are substandard in width by 8-feet. The bridge widths would remain substandard with any rehabilitation project. Additionally, the pier columns of both the north and south bridges are only in fair condition with moderate distress, including vertical cracking with delaminations and spalling in the base of the columns with exposed reinforcing. Due to the amount of concrete repair required at the piers and abutments, a full bridge replacement has comparable annualized costs.

A full bridge replacement will provide 2 new widened bridges with an anticipated design life of 100-years. By replacing the entire bridge, the number of spans can be reduced. The existing pier columns in the US Route 5 median are not adequately protected. By replacing the existing 4-span structure with a new 3-span cantilever bridge that spans US Route 5, the unprotected median pier columns will be eliminated. By decreasing the number of spans, future maintenance needs will also be reduced. Geotechnical borings should be requested early in the design phase to determine the in-situ soil conditions.

Traffic Control:

It is recommended that traffic is maintained on a temporary bridge during construction. Due to the large elevation difference between the northbound and southbound barrels as well as a wide median north of Bridges 28 N&S, a crossover is not ideal at this location. Additionally, the temporary bridge option is the most cost-effective method of traffic maintenance and has the least impact to traffic flow. The temporary bridge can be constructed in the median between Bridge 28N and 28S. That allows the temporary bridge to be used by both barrels of the interstate and reduces overall cost.

VIII. Appendices

Appendix A: Site Pictures Appendix B: Town Map Appendix C: Bridge Inspection Reports Appendix D: Preliminary Geotechnical Information Appendix E: Resource ID Completion Memo Appendix F: Natural Resources Memo Appendix G: Hazardous Waste Sites Appendix G: Hazardous Waste Sites Appendix H: Archaeology Memo Appendix I: Historic Memo Appendix I: Historic Memo Appendix J: Utility Investigation Appendix K: Local Input Appendix K: Local Input Appendix L: Operations Input Appendix M: Crash Data Appendix N: Detour Routes Appendix O: Plans Appendix A: Site Pictures

Bridge 28 North



Rolled beam deterioration at joint



Pier column and cap condition



Pier column and cap condition



Deck and superstructure condition



Abutment Condition (Note saturation due to leaky joint)



Looking north over Bridge 28N



Bridge fascia



Pier Condition



Abutment Condition



Abutment Condition



Abutment Condition



Deterioration around bridge joints



Looking South over Bridge 28N



Pier Condition

Bridge 28 South



Pier column condition



Deterioration around bridge joint



Deterioration at fascia and joint



Bridge deck and superstructure condition



Pier condition



Pier cap condition



Looking South over Bridge 28S



Abutment condition



Pier condition

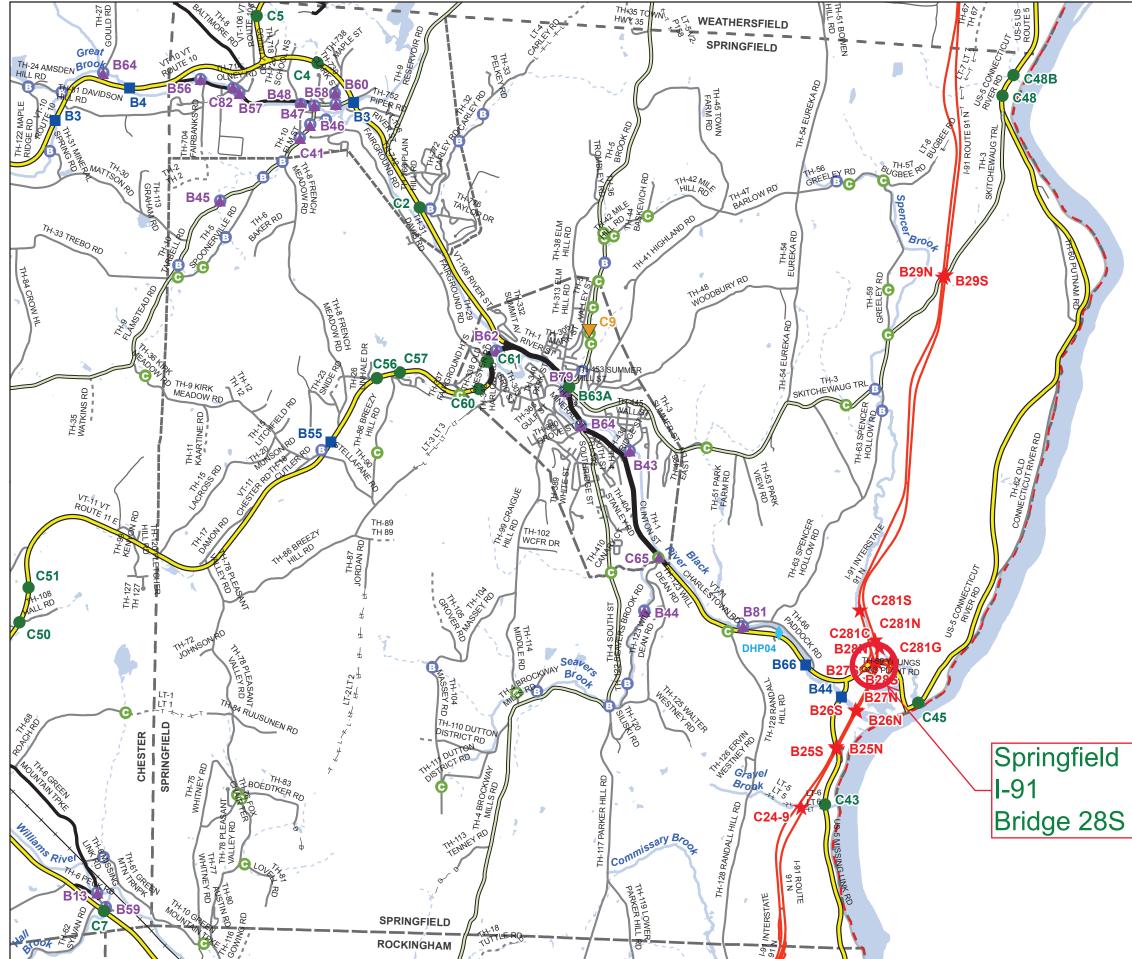


Bridge seat and bearing condition

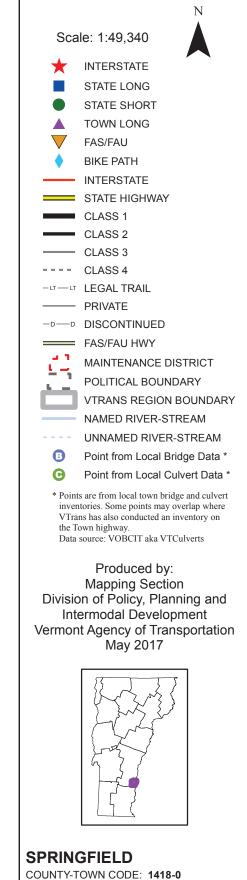


Looking north over bridge 28S

Appendix B: Town Map



This map was funded in part through grants from the Federal Highway Administration, U.S. Department of Transportation. The representation of the authors expressed herein do not necessarily state or reflect those of the U.S. Department of Transportation.



WINDSOR COUNTY DISTRICT #2 District Long Name: Dummerston District VTrans Four Region: Southeast

Appendix C: Bridge Inspection Reports

STRUCTURE INSPECTION, INVENTORY and APPRAISAL SHEET

Vermont Agency of Transportation ~ Structures Section ~ Bridge Management and Inspection Unit

Inspection Report for SPRINGFIELD bridge no.: 0028N District: 2 Located on: I 00091 ML over 191 OVER US 5 approximately I 91 EXIT 7 **Owner:** 01 STATE-OWNED **CONDITION STRUCTURE TYPE and MATERIALS** Deck Rating: 5 FAIR **Bridge Type: 4 SPAN ROLLED BEAM** Superstructure Rating: 5 FAIR Number of Approach Spans: 0000 Number of Main Spans: 004 Substructure Rating: 5 FAIR Kind of Material and/or Design: 3 STEEL Channel Rating: N NOT APPLICABLE Deck Structure Type: 1 CONCRETE CIP Culvert Rating: N NOT APPLICABLE Type of Wearing Surface: 6 **BITUMINOUS** Federal Str. Number: 200091028N14182 Type of Membrane: 2 **PREFORMED FABRIC** Federal Sufficiency Rating: 069 **Deck Protection:** 0 NONE Deficiency Status of Structure: ND APPRAISAL *AS COMPARED TO FEDERAL STANDARDS AGE and SERVICE Bridge Railings: 1 MEETS CURRENT STANDARD Year Built: 1965 Year Reconstructed: 0000 Transitions: 1 MEETS CURRENT STANDARD Service On: 1 HIGHWAY Approach Guardrail: 1 MEETS CURRENT STANDARD Service Under: 1 HIGHWAY Approach Guardrail Ends: 1 MEETS CURRENT STANDARD Lanes On the Structure: 03 Structural Evaluation: 5 BETTER THAN MINIMUM TOLERABLE CRITERIA Lanes Under the Structure: 04 Deck Geometry: 4 MEETS MINIMUM TOLERABLE CRITERIA Bypass, Detour Length (miles): 00 Underclearances Vertical and Horizontal: 3 INTOLERABLE, CORRECTIVE **ACTION NEEDED** ADT: 005500 % Truck ADT: 13 Waterway Adequacy: N NOT OVER WATER Year of ADT: 1999 **GEOMETRIC DATA** Approach Roadway Alignment: 6 EQUAL TO MINIMUM CRITERIA Length of Maximum Span (ft): 0055 Scour Critical Bridges: N NOT OVER WATERWAY Structure Length (ft): 000202 Lt Curb/Sidewalk Width (ft): 0.7 DESIGN VEHICLE, RATING, and POSTING Rt Curb/Sidewalk Width (ft): 0.7 Load Rating Method (Inv): 1 LOAD FACTOR (LF) Bridge Rdwy Width Curb-to-Curb (ft): 42 **Posting Status:** A OPEN, NO RESTRICTION Deck Width Out-to-Out (ft): 47 Bridge Posting: 5 NO POSTING REQUIRED Appr. Roadway Width (ft): 045 Load Posting: 10 NO LOAD POSTING SIGNS ARE NEEDED Skew: 11 **Posted Vehicle:** POSTING NOT REQUIRED Bridge Median: 1 OPEN MEDIAN **Posted Weight (tons):** Min Vertical Clr Over (ft): 99 FT 99 IN Design Load: 4 H 20 Feature Under: HIGHWAY BENEATH X-Ref. Route: US5 **INSPECTION and CROSS REFERENCE STRUCTURE** Min Vertical Underclr (ft): 14 FT 11 IN Insp. Date: 052018 Insp. Freq. (months) 24 X-Ref. BrNum: 0044B

INSPECTION SUMMARY and NEEDS

5/17/2018 This structure should be considered for a deck replacement project, eliminating the joint over pier 2 and new joints installed over the abutments. Concrete repairs are needed to pier 2 and abutment 2, removing all loose concrete and delams. The west fascia beam ends over pier 2 need to have steel repairs made. New bearings should be set in areas below the joints, mostly along the west fascia. JW/MC

5/16/2016 This structure needs to have concrete repairs to the curbs with new seals installed especially in the ends surrounding the joints. The finger plate joints should be considered for replacement with Vermont joints and should extended to the fascias with scuppers installed. Concrete repairs are needed to abutment 2, piers 2 and 3 with all loose concrete/delams removed and then patched. JW/AC

5/15/2014 Curbs need major repair soon. Weep tubes should be extended below the beams. Bearing have been greased however the heavy rusting should have been cleaned. the bearing on abutment #1 side under beam #1 and #5 should be cleaned and reset as bearing #5 on abut#1 could fail. Erosion in the slopes at the drain troughs should be repaired. Beams should be spot cleaned and painted. ~FRE/TJB

5/00/0010 Cunte should be slowed and notshed alone with the solutions on view #2 EDE/OIII

	PECTION, INVENTORY and APPRAISAL SHEET tion ~ Structures Section ~ Bridge Management and Inspection Unit
Inspection Report for SPRINGFIELD Located on: 100091 ML over 191 OVER US	bridge no.:0028SDistrict:25.5approximately191 EXIT 7Owner:01 STATE-OWNED
CONDITION Deck Rating: 6 SATISFACTORY Superstructure Rating: 7 GOOD Substructure Rating: 6 SATISFACTORY Channel Rating: N NOT APPLICABLE Culvert Rating: N NOT APPLICABLE Federal Str. Number: 200091028S14182 Federal Sufficiency Rating: 081	STRUCTURE TYPE and MATERIALSBridge Type: 4 SPAN ROLLED BEAMNumber of Approach Spans: 0000Number of Main Spans: 004Kind of Material and/or Design: 3STEELDeck Structure Type: 1CONCRETE CIPType of Wearing Surface: 6BITUMINOUSType of Membrane: 2PREFORMED FABRICDeck Protection: 0NONE
Deficiency Status of Structure: ND AGE and SERVICE Year Built: 1965 Year Reconstructed: 0000 Service On: 1 HIGHWAY Service Under: 1 HIGHWAY Lanes On the Structure: 02 Lanes Under the Structure: 04 Bypass, Detour Length (miles): 00 ADT: 005375 % Truck ADT: 13 Year of ADT: 1998	APPRAISAL*AS COMPARED TO FEDERAL STANDARDSBridge Railings: 1MEETS CURRENT STANDARDTransitions: 1MEETS CURRENT STANDARDApproach Guardrail: 1MEETS CURRENT STANDARDApproach Guardrail Ends: 1MEETS CURRENT STANDARDStructural Evaluation: 6EQUAL TO MINIMUM CRITERIADeck Geometry: 4MEETS MINIMUM TOLERABLE CRITERIAUnderclearances Vertical and Horizontal: 4MEETS MINIMUM TOLERABLE CRITERIAWaterway Adequacy: NNOT OVER WATER
GEOMETRIC DATA Length of Maximum Span (ft): 0056 Structure Length (ft): 000207	Approach Roadway Alignment: 7 BETTER THAN MINIMUM CRITERIA Scour Critical Bridges: N NOT OVER WATERWAY
Lt Curb/Sidewalk Width (ft): 0.7 Rt Curb/Sidewalk Width (ft): 0.7 Bridge Rdwy Width Curb-to-Curb (ft): 30 Deck Width Out-to-Out (ft): 35 Appr. Roadway Width (ft): 036 Skew: 12 Bridge Median: 1 OPEN MEDIAN Min Vertical Clr Over (ft): 99 FT 99 IN Feature Under: HIGHWAY BENEATH STRUCTURE Min Vertical Underclr (ft): 17 FT 04 IN	DESIGN VEHICLE, RATING, and POSTINGLoad Rating Method (Inv):1LOAD FACTOR (LF)Posting Status:AOPEN, NO RESTRICTIONBridge Posting:5NO POSTING REQUIREDLoad Posting:10NO LOAD POSTING SIGNS ARE NEEDEDPosted Vehicle:POSTING NOT REQUIREDPosted Weight (tons):Design Load:Design Load:5HS 20INSPECTION and CROSS REFERENCEX-Ref. Route:US5Insp. Date:052018Insp. Freq. (months)24X-Ref. BrNum:0044A

INSPECTION SUMMARY and NEEDS

5/18/2018 This structure should be considered for a deck replacement project, or new fascias installed to replace the heavily deteriorated cubs and affected soffit below. New joints over the abutments should be installed as well. The beams need general cleaning and painting. JW/MC

5/16/2016 This structure needs to have concrete repairs to the curbs with new seals installed especially in the ends surrounding the joints. The finger plate joints should be considered for replacement with Vermont joints and should extended to the fascias with scuppers installed. JW/AC

5/15/2014 Curbs should be cleaned of all loose material and patched. Beams should be spot cleaned and painted. ~FRE/TJB

5/22/2012 Curbs should be cleaned and patched along with the spalling in the fascias. ~FRE/SJH

04/12/10 Left top rail near abutment No.2 needs repair or replacement. Column No.1 of pier No.2 needs repair. The curb areas on both sides are in need of repairs. PLB

Appendix D: Preliminary Geotechnical Information

AGENCY OF TRANSPORTATION

To:	Nick Wark, P.E., P.I.I.T. Program Manager
From:	ASA August Arles, Geotechnical Engineer, via Callie Ewald, P.E., Geotechnical Engineering Manager
Date:	February 24 th , 2020
Subject:	Springfield IM 091-1(83) Preliminary Geotechnical Information

1.0 INTRODUCTION

As requested, we have completed the preliminary geotechnical investigation of Bridges 28N/S on Interstate 91 over VT Route 11 in the Town of Springfield. Bridges 28N/S are four-span rolled beam steel bridges that are part of the Exit 7 interchange. The subject project consists of replacing or rehabilitating the existing structures. This review included the examination of as-built record plans, in-house historical boring log files, well log data, and hazardous site information on file at the Vermont Agency of Natural Resources (ANR), as well as published geologic maps relating to surficial and bedrock data.

2.0 SUBSURFACE INFORMATION

2.1 Published Geologic Data

Mapping conducted in 1970 for the Surficial Geologic Map of Vermont shows the project site consists of glaciolacustrine deposits of littoral sediment, predominantly sand (Doll, 1970).

According to the Bedrock Map of Vermont from 2011, published by the USGS and State of Vermont, the project site is underlain with bedrock consisting of slate and quartzite of the Waits River Formation and is close to the boundary of schist and conglomerate of the Waits River Formation (Ratliffe, et. al, 2011).

The Geotechnical Engineering Section maintains a GIS based historical record of subsurface investigations, which contains electronic records for the majority of borings completed in the past 10 years. An exploration of this database revealed borings from a previous project within a 0.5-mile radius. Four borings were advanced at the intersection of VT Route 11 and Missing Link Rd in February 2017 for the Springfield STP 016-2(23) project. In general, soils encountered during this investigation consisted of varying amounts of silty-sand, gravelly-sand, and silts. Bedrock was encountered between depths of 10.1 feet and 23.0 feet, corresponding to elevations of 299.6 ft and 289.5 ft, respectively as was classified as moderately to medium hard phyllite, and medium hard schist. Ground water was encountered in all borings and ranged from five feet to fifteen feet below ground surface elevation. The boring logs and boring location plan from this project are attached.

2.2 Water Well Logs

The Vermont ANR maintains a record of private and public wells drilled in their Atlas database. Published online, these logs may provide general characteristics of the soil strata and depth to bedrock in the area. The three closest logs of wells, TAG 290, WRN 102, and WRN 276, were located approximately 909 feet, 1067 feet, and 1879 feet from the project site and reported bedrock at a depth of 8 feet, 14 feet, and 3 feet respectively.

2.3 Hazardous Materials and Underground Storage Tanks

The ANR Atlas also maintains a database of all known hazardous waste sites and underground storage tanks. According to their published data there are five sites within a 0.5-mile radius, consisting of four hazardous waste generators and two hazardous sites, and two underground storage tanks. The project itself does not lie on a hazardous site, and there is no anticipated impact on the project from the surrounding sites.

2.4 Record Plans

Record plans from the intersection construction dated 1965 were also reviewed as part of this investigation. The record plans included a layout sheet and a plan and elevation sheet for the Bridge 28 Southbound. The P&E detail sheet indicates that the concrete abutments for the southbound bridge are founded on 3 rows of 12BP53 steel piles with a design load of 24 tons and an estimated length of 30 feet. The design bottom of pile cap elevation for Abutment's No.1 and No. 2 are shown as 353.15 ft and 353.11 ft, respectively. The P&E sheet also details that the reinforced concrete piers for the southbound bridge, consisting of three 3-ft diameter columns per pier, are founded on spread footing foundations with a design bottom of footing elevation of 328 ft at Pier No.1, and an elevation of 334 ft for Piers No. 2 and 3.

3.0 FIELD OBSERVATIONS

A site investigation was not conducted by Geotechnical Section staff however photos from bridge inspection reports and satellite imagery were reviewed to evaluate feasibility of boring operations and assess general site conditions as they relate to the proposed project.

No overhead obstructions were observed along I-91 that would interfere with any potential boring operations. Borings advanced for the bridge abutments can likely be located in the median of I-91 and from either the side slopes of I-91 or from the roadway of VT Route 11 and the adjacent slopes. For borings advanced for potential piers, if drilling is to be conducted from the roadway of VT Route 11, then borings will likely need to be located outside of the footprint of the existing bridge structures due to limited overhead clearance under the bridges. If borings are deemed to be required close to the center of the existing pier locations, then borings could be advanced through the bridge deck from the travel lanes of I-91 which would likely require significant traffic control coordination, closure of one lane of the interstate, and possibly closure of one lane of VT Route 11.

Bedrock was not visible in any of the available imagery. Bridge abutments were armored with stone fill as shown in Figure 3.1. Figure 3.2 through Figure 3.4 illustrate the overhead clearance limitations along VT Route 11 that may restrict drilling from directly beneath the existing structures.



Figure 3.1: Stone fill armoring at bridge abutment underneath Interstate 91 Bridge 28 Southbound. [Inspection photo dated 2018]



Figure 3.2: Facing I-91 Bridge 28 Southbound south abutment; note limited overhead clearance for drilling operations under existing bridge. [Inspection photo dated 2018]



Figure 3.3: Facing I-91 Bridge 28 Southbound north abutment; note limited overhead clearance for drilling operations under existing bridge deck. [Inspection photo dated 2016]



Figure 3.4: Facing east, Bridge 28 Southbound. [Inspection photo dated 2016]

4.0 **RECOMMENDATIONS**

4.1 Preliminary Foundation Alternatives

Based on this information, possible foundation options for bridge replacements include the following:

Abutments

- Reinforced concrete abutments on spread footings
- Pile caps on a single row of H-Piles
- Reinforced concrete abutments founded on piles with mechanically stabilized earth (MSE) walls

Piers

- Reinforced concrete piers on spread footings
- Pile caps supported by H-Piles
- Pier columns supported on drilled shafts

4.2 Proposed Subsurface Investigation

Once proposed alignments for the replacement bridges are chosen as well as preferred foundation alternatives, we recommend assessing the existing subsurface information and developing a subsurface investigation program that augments the existing information to verify the subsurface conditions at the site including, but not limited to, the soil properties, groundwater conditions, and depth to bedrock. If drilled shafts are contemplated, final borings should be aligned with the shaft location(s) to the degree possible given access restrictions.

5.0 CLOSING

When a design alternative, as well as a preliminary alignment has been chosen, the Geotechnical Engineering Section can assist in designing a subsurface investigation that efficiently gathers adequate information for the alternative chosen.

If you have any questions or would like to discuss this report, please contact us by phone at (802) 828-2561.

6.0 **REFERENCES**

Doll, C. G., 1970, Surficial Geologic Map of Vermont, Vermont Geological Survey, Montpelier, VT.

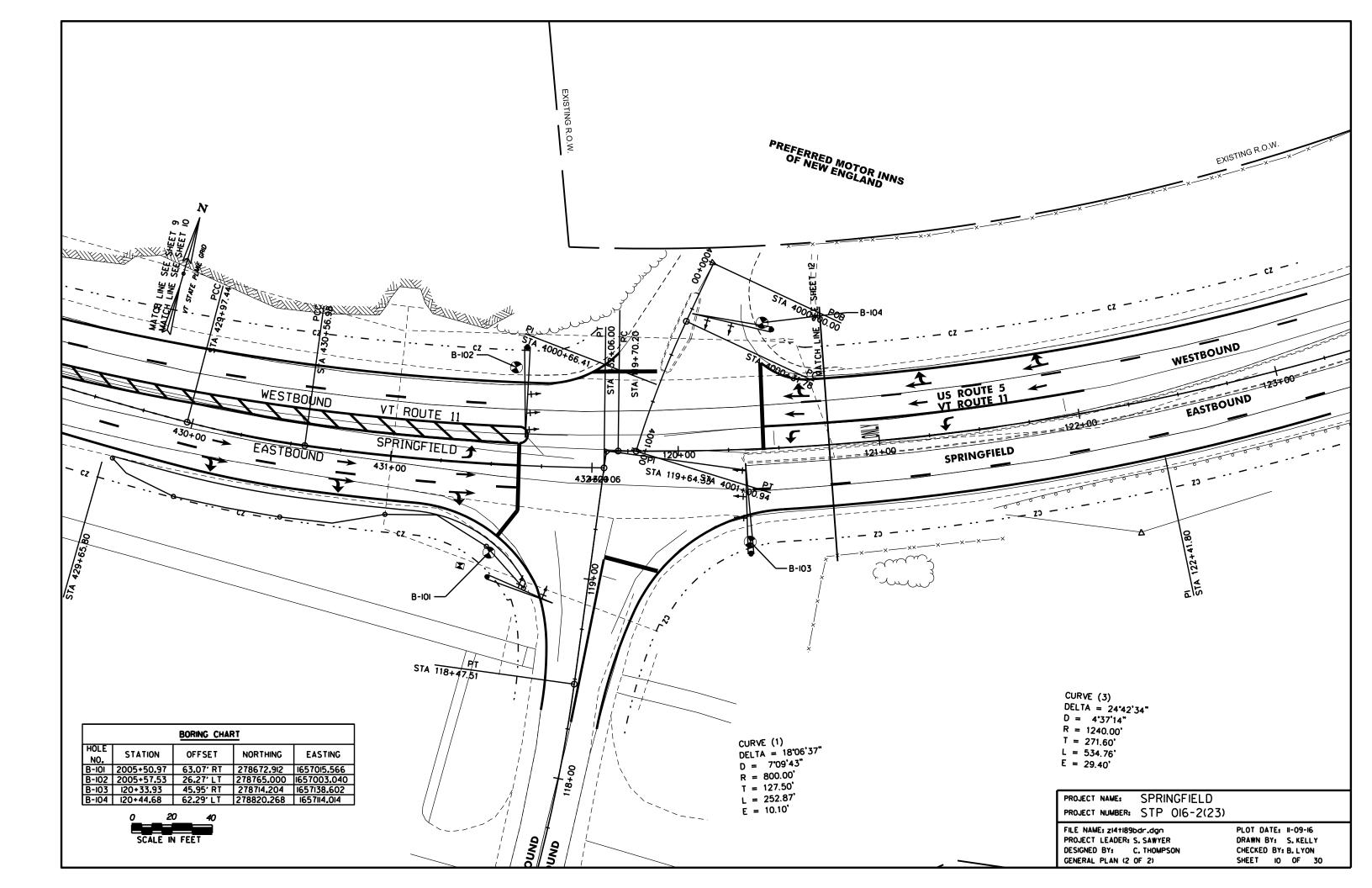
Ratcliffe, N. M., Stanley, R. S., Gale, M. H., Thompson, P. J., Walsh, G. J., 2011, Bedrock Geologic Map of Vermont, Vermont Geological Survey, Montpelier, VT.

Vermont Agency of Natural Resources Department of Environmental Conservation, Natural Resources Atlas, www.anr.vermont.gov/maps/nr-atlas%20, accessed 2/10/2020.

Enclosures: Boring Location Plan (1 Page) Boring Logs (4 Pages)

cc: Laura Stone, P.E., P.I.I.T. Project Manager Electronic Read File/MG Project File/CEE AJA

Z:\Highways\CMB\GeotechEngineering\Projects\Springfield IM 091-1(83)\REPORTS\Springfield IM 091-1(83) Preliminary Geotechnical Report.docx



V	Trans	STATE OF VERMONT AGENCY OF TRANSPORTA CONSTRUCTION AND MATERIALS BUREAU CENTRAL LABORATOR		BORING LOG Springfield STP 016-2(23) US-5 VT-11						Boring Page N Pin No Checke	lo.: .:	1 of 1 14t189		
Date S	Started: G NAD83:		Type: I.D.: Hamm Hamm	er Wt: er Fall:	Casing H.S.A 3.25 ir N.A. N.A.	<u> </u>	mpler SS 5 in 0 lb. 0 in.	Da 02/01	te D	dwater Depth (ft) 6.3	Observ N W.T. d	lotes		
Statio Grour	nd Elevation	<u> </u>		er/Rod T CME 45		Auto/A	= 1.42							
Depth (ft)	Strata (1)	CLASSIFICATION OF MAT (Description)	ERIALS			Run (Dip deg.)	Core Rec. % (RQD %)	Drill Rate minutes/ft	Blows/6" (N Value)	Moisture	Gravel %	Sand %)0 : L	
-		A-1-b, GrSa, brn, Moist, Rec. = 0.5 ft, Lab N plant material was within sample	ote: Some	e decomp	oosing				3-3-3- (6)		3 34.8	47.5	17	
-		A-4, SaSi, brn, Moist, Rec. = 1.7 ft							2-2-2- (4)			48.1		
5 -		A-2-4, Sa, brn, Moist, Rec. = 1.2 ft A-1-a, SaGr, brn, Moist, Rec. = 0.3 ft							3-2-3- (5) 4-4-4-		4 0.1 2 65.1			
-		A-4, Si, brn, Moist, Rec. = 1.7 ft							(8) 3-2-3- (5)					
10 — - -		A-4, GrSi, brn, Moist, Rec. = 0.4 ft							(3) 3-3-3- (6)	-4 24.	5 25.7	19.8	54	
- 15 — - -		A-4, Si, brn, Moist, Rec. = 1.8 ft, Lab Note: S sample. Sample tested non-plastic	Some clay	was with	nin				1-2-1- (3)	-1 36.	8	1.4	98	
- 20 — -		A-4, Si, gry, Moist, Rec. = 2.0 ft, Lab Note: S sample. Sample tested non-plastic	Some clay	was with	in				1-1-2- (3)	-2 32.	3 0.1	16.4	83	
- - 25 - - -		23.0 ft - 28.0 ft, Gray to dark gray, Carbonaceous muscovite-quartz-plagioclase PHYLLITE, with pyrite. Moderately hard, Unweathered, Fair rock, NX, RMR=60					92) (80)	4 3 3 3 2		Top c	of Bedro	ock @	23.0	
- 30 — -		28.0 ft - 33.0 ft, Gray to dark gray, Carbonaceous 2 muscovite-quartz-plagioclase PHYLLITE, with pyrite. Rust stained (80) sub-vertical joint from 31.25 feet to 32.70 feet with secondary rineral precipitation in vugs. Medium hard, Slightly weathered, Fair rock, NX, RMR=52 2						2 3 2 2 2 4						
- 35 —		Hole stopped @ 33.0	ft											
-		Remarks: Hole collapsed at 25.0 feet.												
-		1. Changed to wash bore drilling at 23 feet d	lue to susp	pected be	ed rock.									

2.5 (4) (4) 2.6 (4) 9-8-9-11 3.0 A-1-b, SaGr, bm, Moist, Rec. = 1.2 ft 9-8-9-11 5.0 Field Note:, NXDC, Cleaned out casing 9-20-15 7.5 Field Note:, NXDC, Cleaned out casing 9-7,7-4 A-1-b, GrSa, bm, Moist, Rec. = 0.3 ft 9-7,7-4 14.5 7.5 Field Note:, NXDC, Cleaned out casing 9-7,7-4 A-3, GrSa, bm, Moist, Rec. = 0.7 ft, Lab Note: Broken rock was within sample 5-2-15 Field Note:, NXDC, Cleaned out casing 10.0 Visual Description:, Broken Rock, gry, Moist, Rec. = 0.1 ft 10.1 ft : 15.1 ft, Gray, Carbonaceous muscovite-quartz-plagioclase PHYLLITE, with pryte. Prenetrative rust staining along joints. Medium hard, Slightly weathered, Fair rock, NX, RMR=46 15.0 15.1 ft - 20.1 ft, Light gray to gray, Carbonaceous muscovite-quartz-plagioclase gneissis. SCHIST, with pryte. Rust and suffur stained sub-vericial pint from 15.2 foct 17.0 ft with secondary mineral precipitation in vugs. Medium hard, Slightly to moderately weathered. Poor rock, NX, RMR=36 6 10.0 Hole stopped @ 20.1 ft 5 22.5 Hole stopped @ 20.1 ft 1. Statistication have preceded at 6.0 feet. 1. Statistication have preceded approximate types. Thereton may be graved.			STATE OF VERMONT		BC	RING I	_OG			Bori	ng No	D.:	B-1	02
Differ LABORATORYUN to the super-transmission of the super-transmission	(V									Pag		1 of 1		
Late the Checked by:StructureChecked by:StructureBoring Crew:Emerson, Garrow, OldenType:WBSsGroundwater ObservationsDate Started:12/28/17Date Finished:12/28/17Station:Groundwater ObservationsVTSPG NAD83:N 278765.00 ft E 1657003.00 ftHammer Fail:NA.140 lb.DateDateStation:431+60Offset:48.5 LTHammer Fail:NA.30 in12/28/17StateW.T. after drillingGround Elevation:309.7 ftCLASSIFICATION OF MATERIALS $\overline{0}^{\frac{10}{9}}$ $\overline{0}^{\frac{10}$	1	MATERIALS BOREAU 3										14t18	9	
Boing Crew:Emerson Garrow, Olden I 1228/17Type:WB 4 inSS 1.5 inDate Standard (ft)Date Started:1228/17Date Finished:1228/17Date Finished:1228/17S.8U.T. after drillingVTSPC NAD83:N 278765.00 ftE 1657003.00 ftHammer KeilNA.140 lb. Hammer Fail:NA.140 lb. Hammer Fail:1228/17S.8W.T. after drillingGround Elevation:309.7 ftCLASSIFICATION OF MATERIALS $ggg garge gar$								1				-	_	'M
Date Started: 12/28/17 Date Finished: Date Finishe: Date Finishe:	Boring	g Crew:	Emerson, Garrow, Olden	Type [.]		-								
VTSPC NAD83: N278765.00 ft E 1657003.00 ft Station: 431+60	Date	Started: _	12/28/17 Date Finished: 12/28/17					Dat	ie [h	N	otes	
Station:A1-b. GrSa, brn, Moist, Rec. = 1.2 ft $f = 0$ <td>VTSP</td> <td>G NAD83:</td> <td>N 278765.00 ft E 1657003.00 ft</td> <td></td> <td></td> <td></td> <td></td> <td>12/28</td> <td>/17</td> <td></td> <td>M</td> <td>/.T. af</td> <td>ter dril</td> <td>lling</td>	VTSP	G NAD83:	N 278765.00 ft E 1657003.00 ft					12/28	/17		M	/.T. af	ter dril	lling
Ground Elevation:309.7 ftRig:CME 45C SKID $C_{E} = 1.42$ $\frac{1}{90}$ $\frac{1}{10}$	Statio	on: <u>43</u>	01+60 Offset: 48.5 LT											
End End CLASSIFICATION OF MATERIALS (Description) End	Grour	nd Elevatio	n:309.7 ft		· · _									
2.5 A-1-b, GrSa, brn, Moist, Rec. = 1.3 ft 1.1-3-7 12.1 29.0 58.7 12.1 2.5 A-1-b, GrSa, brn, Moist, Rec. = 1.2 ft 9-8-9-11 11.5 30.0 51.5 18.1 2.5 A-1-b, GrSa, brn, Moist, Rec. = 1.2 ft 9-8-9-11 11.5 30.0 51.5 18.1 5.0 A-1-b, GrSa, brn, Moist, Rec. = 1.4 ft 14 9-20-15- 10.8 42.9 39.0 18.1 7.5 Field Note:, NXDC, Cleaned out casing 9-7.7-4 14.5 24.1 68.8 7.1 7.5 Field Note:, NXDC, Cleaned out casing 9-7.7-4 14.5 24.1 68.8 7.1 10.0 Visual Description:, Broken Rock, gry, Moist, Rec. = 0.1 ft 15 18.4 26.7 67.9 5.4 10.0 Visual Description:, Broken Rock, gry, Moist, Rec. = 0.1 ft 10.1 165-751 169 4 R@ 1* Top of Bedrock @ 10.1 112.5 12.5 3 3 3 3 3 3	_	(1)				g.)	с. % %)	ite s/ft			e%	%	%	%
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Depth (ft)	Strata		RIALS		Run (Dip de	Core Rec (RQD	Drill Ra minutes	Blows/ (N Valu		Moistu Content	Gravel	Sand ⁶	Fines
$\begin{array}{c} 2.5 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $	-		A-1-b, GrSa, brn, Moist, Rec. = 1.3 ft								12.1	29.0	58.7	12.3
5.0 Field Note:, NXDC, Cleaned out casing A-1-b, GrSa, brn, Moist, Rec. = 0.3 ft 7.5 Field Note:, NXDC, Cleaned out casing A-3, GrSa, brn, Moist, Rec. = 0.7 ft, Lab Note: Broken rock was within sample Field Note:, NXDC, Cleaned out casing 10.0 Visual Description:, Broken Rock, gry, Moist, Rec. = 0.1 ft 10.1 ft - 15.1 ft, Gray, Carbonaceous muscovite-quartz-plagioclase PHYLLITE, with pyrite. Penetrative rust staining along joints. Medium hard, Slightly weathered, Fair rock, NX, RMR=46 12.5	2.5 -		A-1-b, GrSa, brn, Moist, Rec. = 1.2 ft								11.5	30.0	51.5	18.5
i i	- 5.0 -								14		10.8	42.9	39.0	18.1
7.5 Field Note:, NXDC, Cleaned out casing A-3, GrSa, brn, Moist, Rec. = 0.7 ft, Lab Note: Broken rock was within sample Field Note:, NXDC, Cleaned out casing 10.0 Visual Description:, Broken Rock, gry, Moist, Rec. = 0.1 ft 10.1 Visual Description:, Broken Rock, gry, Moist, Rec. = 0.1 ft 10.1 Visual Description:, Broken Rock, gry, Moist, Rec. = 0.1 ft 10.1 Visual Description:, Broken Rock, gry, Moist, Rec. = 0.1 ft 10.1 10.1 ft - 15.1 ft, Gray, Carbonaceous muscovite-quartz-plagioclase PHYLLITE, with pyrite. Penetrative rust staining along joints. Medium hard, Slightly weathered, Fair rock, NX, RMR=46 3 3										-4	14.5	24.1	68.8	7.1
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PHYLLITE, with pyrite. Penetrative rust staining along joints. Medium hard, Slightly weathered, Fair rock, NX, RMR=46 12.5-	10.0-						100	4	R@1		n of F	Redro	_k @ 1	10 1 f
	-		PHYLLITE, with pyrite. Penetrative rust staining	ng along	joints.	(65-75)	(69)		(R)		,p oi i			
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15.0 15.1 ft - 20.1 ft, Light gray to gray, Carbonaceous muscovite-quartz-plagioclase gneissic SCHIST, with pyrite. Rust and sulfur stained sub-vertical joint from 15.2 feet to 17.0 feet with secondary mineral precipitation in vugs. Medium hard, Slightly to moderately weathered, Poor rock, NX, RMR=36 2 100 5 17.5 6 6 6 6 20.0 Hole stopped @ 20.1 ft 5 6 22.5 Notes 1. Stratification lines represent approximate boundary between material types. Transition may be gradual. 2. N values have not been corrected for harmer energy. C ₆ is the harmer energy correction factor.	-													
15.1 ft - 20.1 ft, Light gray to gray, Carbonaceous muscovite-quartz-plagioclase gneissic SCHIST, with pyrite. Rust and sulfur stained sub-vertical joint from 15.2 feet to 17.0 feet with secondary mineral precipitation in vugs. Medium hard, Slightly to moderately weathered, Poor rock, NX, RMR=36 2 100 5 17.5 6 5 6 20.0 Hole stopped @ 20.1 ft 5 22.5 1. Stratification lines represent approximate boundary between material types. Transition may be gradual. 2. Notes: 1. Stratification lines represent approximate boundary between material types. Transition may be gradual.	15.0-													
sulfur stained sub-vertical joint from 15.2 feet to 17.0 feet with secondary mineral precipitation in vugs. Medium hard, Slightly to moderately weathered, Poor rock, NX, RMR=36 6 5 20.0 Hole stopped @ 20.1 ft Remarks: Hole collapsed at 6.0 feet.	-	<i>V////</i>	muscovite-quartz-plagioclase gneissic SCHIS	T, with p	yrite. Rust and			5						
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20.0 Hole stopped @ 20.1 ft Bemarks: Hole collapsed at 6.0 feet. 1. Stratification lines represent approximate boundary between material types. Transition may be gradual. 2. N Values have not been corrected for hammer energy. C _E is the hammer energy correction factor.	-	Y <i> </i>						5						
Hole stopped @ 20.1 ft Bemarks: Hole collapsed at 6.0 feet. Notes: 1. Stratification lines represent approximate boundary between material types. Transition may be gradual. 2. N Values have not been corrected for hammer energy. C _E is the hammer energy correction factor.	20 0 -													
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		STATE OF VERMONT			BOR	NG LOG			Bor	ing No	0.:	B-1	03	
										Page No.: <u>1 of 1</u>				
	MATERIALS BUREAU STP 016-2(23)									Pin No.:			14t189	
		CENTRAL LABORATORY			US	-5 VT-11			Che	ecked	By:	SF	PM_	
Borin	a Crew:	Garrow, Emerson	_		Casing	Sampler		Grour	ndwa	ater O	bserva	ations		
	-	1/31/17 Date Finished: 1/31/17	Type: I.D.:		H.S.A. 3.25 in	<u></u> 1.5 in	Da	te I	Dept	h	N	otes		
	PG NAD83:		Hamm	er Wt:	N.A.	140 lb.	01/31	1/17	(ft) 15.6		1	uring d	rilling	
Statio	on: 12	0+34 Offset: 45.9 RT		er Fall:	N.A.	30 in.	01/3		15.0		v. i . u	uning u	ming	
Grou	nd Elevatio			er/Rod Ty CME 45		$\frac{\text{uto/AWJ}}{C_{\text{E}} = 1.42}$				-				
				0	<u> </u>	<u></u>								
Depth (ft)	Strata (1)	CLASSIFICATION		ERIALS				Blows/6" (N Value)		Moisture Content %	Gravel %	Sand %	Fines %	
ے م	Stra	(Descri	iption)					Blo		Cont	Gra	Sar	Ë	
	0.1,0.1	A-2-4, SiGrSa, brn, Moist, Rec. = 1.0 ft						4-2-2	2-4		23.1	55.3	21.6	
								(4)						
		A-4, SaSi, brn, Moist, Rec. = 1.6 ft						2-2-3	3-3	26.7	1.5	33.7	64.8	
								(5)		20.7	1.0	00.7	04.0	
	1///									00.4		00.0	70.0	
5 -		A-4, SaSi, brn, Moist, Rec. = 1.6 ft						2-2-2 (4)		29.1	0.1	23.9	76.0	
Ĭ	<u> </u>]						
	0,0	A-2-4, SiSa, brn, Moist, Rec. = 1.9 ft						4-3-3		18.1	0.3	64.7	35.0	
		A-4, SiSa, brn, Moist, Rec. = 1.7 ft						2-3-5	5-5	24.8	4.2	58.7	37.1	
10 -	0 () 0	A-1-b, GrSa, brn, Moist, Rec. = 1.2 ft 7-7-7-10 10.2 30.2 57.0 12								12.8				
	0	A-1-b, GrSa, brn, Molst, Rec. = 1.2 It (14) (14) (14) (12.6)								12.0				
15														
15 -	6777	A-4, SiSa, brn, MTW, Rec. = 1.0 ft						2-2-2 (4)	2-3	29.9	3.7	55.0	41.3	
								(')						
								-						
	-													
8/18	-													
20 -	V1,1/	A-4, Si, brn, MTW, Rec. = 1.7 ft						1-1-2	2-1	39.2	0.3	3.0	96.7	
GDT	<i>K///</i>	,,,,						(3)		23.L	0.0			
AOT								_						
INOM														
VER														
GPJ														
25 -	777.1	A-4, Si, brn, MTW, Rec. = 1.8 ft, Lab Note: So	ome clay	was with	in sample.	Sample tes	ted	1-2-2 (4)	2-4	37.0		2.6	97.4	
016-2	1///	non-plastic						(4)						
- 02 - 25 - 02 - 25 Note: - 02 - 016-2(23),GPJ VERMONT AOT.GDT 10/18/18 - 02 - 25 -		Hole stoppe	d @ 27.0) ft				1			l		L	
FIELC	-													
RING	-	Remarks:												
S 30 -	-	Hole collapsed at 12.8 feet.												
	1 Stratificatio	on lines represent approximate boundary between material types.	Transition	nav he gradu	al									
Notes:	2. N Values h	and the tepresent approximate boundary between material types, have not been corrected for hammer energy. $C_{\rm E}$ is the hammer en- el readings have been made at times and under conditions stated.	nergy correct	tion factor.		actors than those	e presen	t at the tir	ne me	asurem	ients we	re made		
BO							F. 5501							

V	Trans	STATE OF VERMONT AGENCY OF TRANSPORTA CONSTRUCTION AND MATERIALS BUREAU CENTRAL LABORATOR		BORING LOG Springfield STP 016-2(23) US-5 VT-11					oring N age No n No.: heckeo).: _	<u>B-1</u> 1 of 14t18	1
Borino	g Crew:	Emerson, Garrow, Olden	-		Casing	Sampler		Groundv	vater C	bserv	ations	
		<u>12/27/17</u> Date Finished: <u>12/27/17</u>	Type: I.D.:		<u>WB</u> 4 in	<u>SS</u> 1.5 in	Dat	e De	pth t)	N	lotes	
VTSP	G NAD83:	N 278820.30 ft E 1657114.00 ft	Hamm		N.A.	140 lb.	12/27			N.T. a	fter dri	lling
Statio	on: <u>12</u>	0+45 Offset: <u>62.4 LT</u>		er Fall: er/Rod T	<u>N.A.</u> vpe: A	<u> 30 in. </u> uto/AWJ						
Grour	nd Elevatior	n: <u>314.0 ft</u>	Rig:	CME 45	C SKID	$C_{\rm E} = 1.42$						
Depth (ft)	Strata (1)	CLASSIFICATIC (Desc	ON OF MAT	FERIALS				Blows/6" (N Value)	Moisture Content %	Gravel %	Sand %	Fines %
	0	A-2-4, SiSa, Rec. = 1.2 ft						2-2-3-7	14.5		61.0	20
-	0,0							(5)				
-	0.0	A-2-4, SiSa, Rec. = 1.4 ft						5-7-7-6	14.7	2.3	74.7	23
-								(14)				
-		A-2-4, SiSa, Rec. = 2.0 ft						5-5-4-6	26.4	0.7	70.6	28.
5 -	/ 0/ 0							(9)				
-		A-1-b, GrSa, Rec. = 1.1 ft						7-10-16-	6.1	43.4	46.4	10.
-								16 (26)				
-	<u>890</u> 8	Field Note:, NXDC, Cleaned out casing A-1-b, SaGr, Rec. = 1.0 ft						16-18-	9.2	49.2	39.6	11.
	200							15-10 (33)				
10 -		Field Note:, NXDC, Cleaned out casing Field Note:, No Recovery						6-5-4-4				
-		Field Note., NO Recovery						(9)				
15 -		A-4, Si, Rec. = 1.6 ft, Lab Note: A small amo non-plastic	ount of cla	y was wit	hin sample	e. Sample te	sted	2-2-2-2 (4)	36.8	0.2	3.6	96.2
20 -		Field Note:, No Recovery 2-3-3-3 (6)										
- 25		Field Note:, No Recovery	and @ 27.0) #				3-4-4-3 (8)				
		Hole stopp	bea @ 27.(π								
30 -		Remarks: Hole colapsed at 21.8 feet.										
		on lines represent approximate boundary between material type have not been corrected for hammer energy. C_{F} is the hammer			ual.							

Appendix E: Resource ID Completion Memo



OFFICE MEMORANDUM

AOT - PDB - ENVIRONMENTAL SECTION

RESOURCE IDENTIFICATION COMPLETION MEMO

TO:Laura Stone, Project ManagerFROM:Lee Goldstein, Environmental Specialist, SE RegionDATE:October 28, 2019Project:Springfield IM 091-1(83)-12a568

ENVIRONMENTAL RESOURCES:

Archaeological Site:	Yes	Х	No	See Archaeological Resource ID Memo
Historic/Historic District:	Yes	Х	No	See Historic Resource ID Memo
Wetlands:	Yes	Х	No	See Natural Resource ID Memo
Agricultural Land:				See Natural Resource ID Memo
Fish & Wildlife Habitat:	Yes	Х	No	See Natural Resource ID Memo
Wildlife Habitat Connectivity:				See Natural Resource ID Memo
Endangered Species:				See Natural Resource ID Memo
Stormwater:				See Stormwater Resource ID Memo
6(f) Property:				
Hazardous Waste/				
ANR Urban Background Soils:	Yes	Х	No	See ANR map
USDA-Forest Service Lands:				-
Scenic Highway/ Byway:	Yes	Х	No	
Act 250 Permits:	Yes	Х	No	See ANR map
FEMA Floodplains:	Yes	Х	No	See ANR map
Flood Hazard Area/				
River Corridor:	Yes	Х	No	See ANR map
US Coast Guard:	Yes	Х	No	-
Lakes and Ponds:	Yes	Х	No	See ANR map
303D List/ Class A Water/				
Outstanding Resource Water:	Yes	Х	No	See ANR map
			_	
Surface and Ground Water				
(SPA) Source Protection Area:	Yes	Х	No	See ANR map
Groundwater Classification:	Yes	Х	No	See ANR map
Public Water Sources/				
Private Wells:	Yes	Х	No	See ANR map
Other:	Yes	Х	No	no .dgn created

cc: Project File

Appendix F: Natural Resources Memo



State of Vermont Program Development Division One National Life Drive Montpelier, VT 05633-5001 vtrans.vermont.gov

[phone] 802-279-2562 [fax] 802-828-2334 [ttd] 800-253-0191

To:Project FileFrom:James Brady, VTrans Environmental BiologistDate:October 23, 2019Subject:Springfield IM 091-1(83) - Natural Resource ID

I have completed my natural resource report for the above referenced project. My evaluation has included wetlands, wildlife habitat, agricultural soils and rare, threatened and endangered species.

Bridges 0028N and 0028S, Interstate 91

Wetlands/Watercourses

There are no wetlands or watercourses within the review area.

Wildlife Habitat

There is very limited wildlife habitat at this location.

Rare, Threatened and Endangered Species

The only listed species in the project area is the federally threatened northern long-eared bat. The bridge does not provide useful roosting habitat, so restrictions caused by this animal are unlikely.

Agricultural Soils

There are no mapped agricultural soils in the review area.

Agency of Transportation

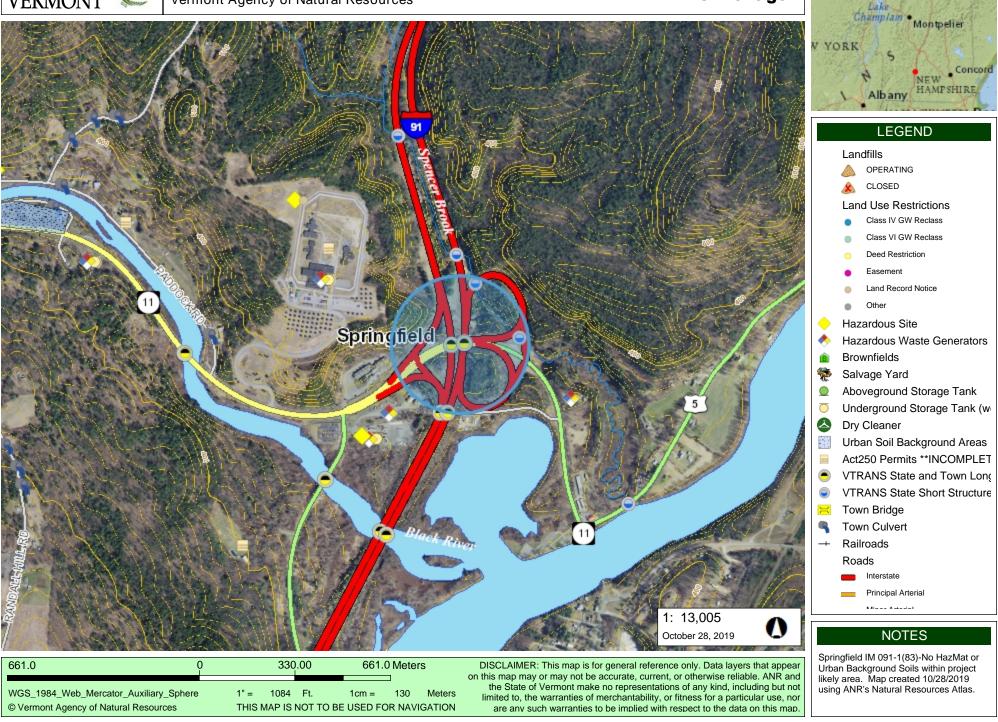
Appendix G: Hazardous Waste Sites



Natural Resources Atlas Vermont Agency of Natural Resources

vermont.gov

VERM ONT



Appendix H: Archaeology Memo



Brennan Gauthier VTrans Senior Archaeologist Vermont Agency of Transportation Project Delivery Bureau Environmental Section 1 National Life Drive Montpelier, VT 05633 tel. 802-279-1460 Brennan.Gauthier@Vermont.gov

To:	Lee Goldstein, VTrans Environmental Specialist
From:	Brennan Gauthier, VTrans Senior Archaeologist
Date:	7/31/2019
Subject:	Springfield IM 091-1(83) Archaeological Resource Identification

lee,

I have completed my field inspection and background research for the pair of I-91 bridges that span Vermont Route 5 in the town of Springfield, Windsor County, Vermont. Although unscoped, I assumed a wide Area of Potential Effect(APE) in order to identify resources that may be worth identifying if the project scope change to include a larger area.

I have concluded that there are no mappable archaeological resources within the area around bridges 28S and 0004S. This area was heavily altered during the construction of I-91 in 1965. Additionally, this project will be cleared as exempt once the Section 106 request is submitted since it involves work on a facility of the Interstate Highway System as per the ACHP notice of 2005.

Please feel free to reach out with any questions or concerns that may arise as part of this process.

Sincerely,

Brennan



Images and Illustrations

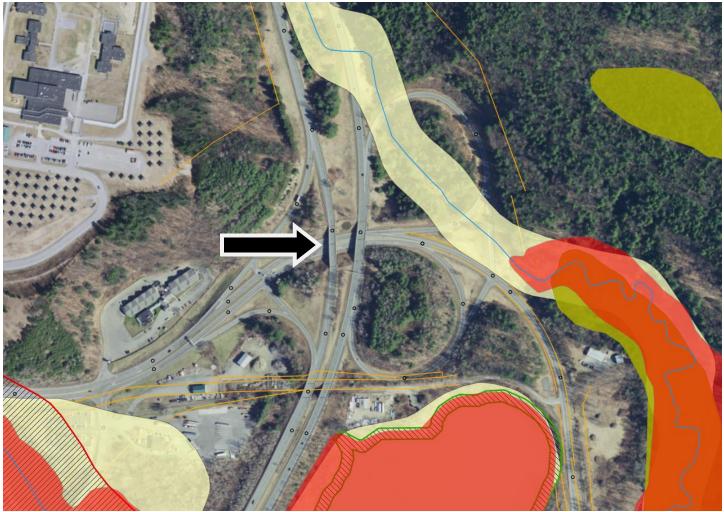


Figure 1: Bridge Locations.



Appendix I: Historic Memo

Goldstein, Lee

From:	Fernandez, Gabrielle
Sent:	Thursday, August 15, 2019 10:53 AM
То:	Goldstein, Lee; Obenauer, Kyle
Subject:	Springfield IM 091-1(83) exempt resource ID

Hi Lee:

This project (Springfield IM 091-1(83)) is considered EXEMPT for above-ground historic resources per the Section 106 Exemption Regarding Effects to the Interstate Highway System adopted by the Advisory Council on Historic Preservation on March 10, 2005. (See Federal Register Vol.70/No.46)

The determination of effect for the overall project will be based on findings for archaeology.

Kyle will update VPINS to note that the project is exempt for above ground resources and Historic review is complete for this project.

Kyle will save this email in the project's NEPA/Specialist Reviews/Historic folder.

Thanks, Gabrielle

Gabrielle Fernandez | AOT Technical Apprentice IV Vermont Agency of Transportation 1 National Life Drive Montpelier, VT 05603 (802) 793-3738



Appendix J: Utility Investigation

Springfield IM 091-1(83)

Existing Utilities within Project Limits Report 08-21-2019 Bridge 28N&S on Interstate I-91 over US 5 in Springfield, Vt.

<u>AERIAL</u>

-No know Aerial Utilities near bridges.

UNDERGROUND

-No know Aerial Utilities near bridges.

MUNICIPAL

There is No known Water and Sewer in vicinity of the bridge.

• Approximately 615 feet to the south of the bridges there is an aerial crossing for a power service. These should not be impacted by the project. FirstLight has buried fiber in bike path/Toonerville Trail approximately 660 feet south of bridges. It is not expected that this will be impacted by the project.

Appendix K: Local Input

Project Summary

This project, IM 091-1(83), focuses on bridge 28S on Interstate 91 South over US Route 5 in Springfield, Vermont. The bridge is deteriorating and is in need of either a major maintenance action or replacement. Potential options being considered for this project include major deck repairs or removal of the existing bridge and replacement with a new bridge placed in the same location. It is possible that VTrans will recommend a road closure and detour traffic off of the interstate for the duration of the work. Efforts will be made to limit the detour to State roads.

Community Considerations

- Are there regularly scheduled public events in the community that will generate increased traffic (e.g. vehicular, bicycles and/or pedestrians), or may be difficult to stage if the bridge is closed during construction? Examples include annual bike races, festivals, parades, cultural events, weekly farmers market, concerts, etc. that could be impacted? If yes, please provide approximate date, location and event organizers' contact info. <u>Not in this location</u>
- Is there a "slow season" or period of time from May through October where traffic is less or no events are scheduled? <u>No</u>
- 3. Please describe the location of the Town garage, emergency responders (fire, police, ambulance) and emergency response routes that might be affected by the closure of the bridge, one-way traffic, or lane closures and provide contact information (names, address, email addresses, and phone numbers. <u>This location is on the far eastern side of the Town and all emergency and essential service facilities are located miles away. As long as Route 5 is not closed during construction there will be no issues traveling east and west. For north bound travel a total closure of the bridges will present an issue for all emergency services and do not think total closure is a viable option.</u>
- 4. Are there businesses (including agricultural operations and industrial parks) or delivery services (fuel or goods) that would be adversely impacted either by a detour or due to work zone proximity? <u>No</u>
- 5. Are there important public buildings (town hall, community center, senior center, library) or community facilities (recreational fields, town green, etc.) close to the project? <u>No</u>
- 6. What other municipal operations could be adversely affected by a road/bridge closure or detour? <u>None other than emergency servicds.</u> As long as Route 5 is not closed during <u>construction there will be no issues traveling east and west.</u>

- Are there any town highways that might be adversely impacted by traffic bypassing the construction on other local roads? Please indicate which roads may be affected and their condition (paved/unpaved, narrow, weight-limited bridges, etc), including those that may be or go into other towns. <u>None. As long as Route 5 is not closed during construction there will be</u> <u>no issues traveling east and west.</u>
- 8. Is there a local business association, chamber of commerce, regional development corporation, or other downtown group that we should be working with? If known, please provide name, organization, email, and phone number.

Springfield On The Move: 96 A Main Street, Springfield, VT 05156 Jessica Martin, Executive Director @ (802) 885-1527 Email: springfieldonthemove@gmail.com

Springfield Regional Chamber of Commerce: 56 Main Street, Suite 2, Springfield, VT 05156 Caitlin Christiana, Executive Director @ (802) 885-2779 Email: springfieldrcoc@vermontel.net

Springfield Regional Development Corporation: 14 Clinton Street, Suite 7, Springfield, VT 05156 Robert "Bob" Flint, Executive Director @ (802) 885-3061 Email: <u>bobf@springfielddevelopment.org</u>

9. Are there any public transit services or stops that use the bridge or transit routes in the vicinity that may be affected if they become the detour route?

The Current: 706 Rockingham Road, Bellows Falls, VT 05101 Phone: (888) 869-6287

The Bus: 158 Spruce Street, Rutland, VT 05701 Phone: (802) 773-3244

<u>Schools</u>

1. Where are the schools in your community and what are their yearly schedules (example: first week in September to third week in June)?

School generally starts the last week in September and finishes the third/fourth week in June.

Springfield School District Administrative Offices: 60 Park Street, Springfield, VT 05156 Dr. Zach McLaughlin, Superintendent @ (802) 885-5141 or (802) 885-5109.

Springfield High School: 303 South Street, Springfield, VT 05156 Bindy Hathorn, Principal @ (802) 885-7900

Riverside Middle School: 13 Fairground Road, Springfield, VT 05156

Steve Cone, Principal @ (802) 885-8490

<u>Union Street School:</u> 43 Union Street, Springfield, VT 05156 Phil Trejo, Principal @ (802) 885-5155

<u>Elm Hill School:</u> 10 Hoover Street, Springfield, VT 05156 Dr. Christine Pereira, Principal @ (802) 885-5154

- Is this project on specific routes that school buses or students use to walk to and from school?
 <u>Yes</u>
- Are there recreational facilities associated with the schools nearby (other than at the school)? There is a bicycle and pedestrian path that terminates about ¼ mile east of this location. The path does not go under the bridges.

Pedestrians and Bicyclists

- 1. Is pedestrian and bicycle traffic heavy enough on VT Route 5 (10A?) that it should be accommodated during construction? <u>No</u>
- Does the Town have plans to construct either pedestrian or bicycle facilities leading up to the bridge? Please provide any planning documents demonstrating this (scoping study, master plan, corridor study, town or regional plan). <u>No</u>
- In the vicinity of the bridge, is there a land use pattern, existing generators of pedestrian and/or bicycle traffic, or zoning that will support development that is likely to lead to significant levels of walking and bicycling? <u>No</u>

Design Considerations

- 1. Are there any concerns with the alignment of the existing bridge? For example, if the bridge is located on a curve, has this created any problems that we should be aware of? <u>No</u>
- 2. Are there any concerns with the width of the existing bridge? No
- 3. Are there any special aesthetic considerations we should be aware of? No
- 4. Are there any known Hazardous Material Sites near the project site? No
- 5. Are there any known historic, archeological and/or other environmental resource issues near the project site? **No**
- 6. Are there any utilities (water, sewer, communications, power) attached to the existing bridge? Please provide any available documentation. <u>No</u>
- 7. Are there any existing, pending, or planned municipal utility projects (communications, lighting, drainage, water, wastewater, etc.) near the project that should be considered? <u>No</u>
- 8. Are there any other issues that are important for us to understand and consider? No

Land Use & Zoning

- Please provide a copy of your existing and future land use map or zoning map, if applicable.
 <u>N/A</u>
- 2. Are there any existing, pending or planned development proposal that would impact future transportation patterns near the bridge? If so, please explain. <u>No</u>
- 3. Is there any planned expansion of public transit or intercity transit service in the project area? Please provide the name and contact information for the relevant public transit provider. <u>No</u>

Communications

- Please identify any local communication outlets that are available for us to use in communicating with the local population. Include weekly or daily newspapers, blogs, radio, public access TV, Facebook, Front Page Forum, etc. Also include any unconventional means such as local low-power FM. <u>The Springfield Reporter (a weekly newspaper) and The Eagle</u> <u>Times (daily newspaper from Claremont) are the local newspapers. WCFR 106.5= radio</u> <u>station. The Town and Police Department have Facebook pages.</u>
- 2. Other than people/organizations already referenced in this questionnaire, are there any others who should be kept in the loop as the project moves forward? **No**

Appendix L: Operations Input

The Structures Section has begun the scoping process for IM 091-1(83), Bridges 28N&S, over US Route 5. These are rolled beam/concrete deck bridges constructed in 1965. The Structure Inspection, Inventory, and Appraisal Sheet (attached) for bridge 28N rates the deck as 5 (fair), the superstructure as 5 (fair), and the substructures as 5 (fair), the Structure Inspection, Inventory, and Appraisal Sheet (attached) for bridge 28N rates the deck as 7 (good), and the substructures as 6 (satisfactory). We are interested in hearing your thoughts regarding the items listed below. Leave it blank if you don't wish to comment on a particular item.

- What are your thoughts on the general condition of these bridges and the general maintenance effort required to keep it in service?
 The deck and abutments are in fair condition, however there is significant rot on the southbound bridge north side, right lane abutment.
- What are your comments on the current geometry and alignment of the bridges (curve, sag, banking, sight distance)?
 The bridge geometry is fine.
- Do you feel that the posted speed limit is appropriate? The speed limit is fine.
- Are the current bridges and approach roadways width adequate for winter maintenance including snow plowing?
 The approaches are adequate, but the southbound bridge could certainly be wider.
- Are the joints salvageable or would you recommend replacement?
 Most of the joints have been replaced with plug joint material and that only lasts a few years.
 The joints that are left have been repaired numerus times with welds and/or new steel plates. All joints need to be replaced.
- Are the railings constantly in need of repair or replacement? What type of railing works best for your district? (We are recommending more and more box beam guardrail on our bridges because of crash-worthiness and compatibility with accelerated projects).
 The railings are fine, however, the concrete they are bolted to is not in the best condition. There is a lot of rot and broken curbing.

- Are you aware of abutting property owners that are likely to need special attention during the planning and construction phases? These could be people with disabilities, elderly, or simply folks who feel they have been unfairly treated in the past.
 There are no abutting property owners here, it is all state land.
- 8. Are you familiar with traffic volumes in the area of this project?
- 9. Do you think a closure with off-site detour and accelerated construction would be appropriate? Do you have any opinion about a possible detour route, assuming that we use State route for State projects and any route for Town projects? Are there locations on a potential detour that are already congested that we should consider avoiding? This bridge goes over Rt 11 which is a 4 lane road (2 lanes headed east and two lanes headed west). There are also the exit 7 north and southbound entrance ramps to take into consideration. I would avoid complete closure and possibly go with a shift to the northbound bridge and visa versa when it is time to replace the southbound.
- Please describe any larger projects that you have completed that may not be reflected on the attached Appraisal sheet, such as deck patches, paving patches, railing replacement with new type, steel coating, etc.
 Joint repairs, removing finger joints and replacing with plug joint material. Grinding out crumbling asphalt in front of finger joints and replacing with new. (Southbound bridge)
- 11. Are there any drainage issues that we should address on this project? None that I know of.
- 12. Are you aware of any complaints that the public has about issues that we can address on this project?
 No section of a sec

None that I know of.

13. Is there anything else we should be aware of?

Appendix M: Crash Data

Vermont Agency of Transportation

General Yearly Summaries - Crash Listing: State Highways and All Federal Aid Highway Systems

WHERE Year of Crash >= 2012 AND Year of Crash <= 2016

*	Reporting Agency/ Incident No.	City/Town	Mile Marker	Crash Date	Time	Weather	Contributing Circumstances	Direction of Collision	Number Of Injuries	Number Of Fatalities	Number Of Untimely Deaths	Direction	Road Group
	VTVSP0400/15D100344	Springfield	41.00	02/02/2015	09.44	[No Weather]	driving	[No Direction of Collision]	0	0	0		SH
	VTVSP0400/15D101873	Springfield	41.00	06/13/2015		[No Weather]		[No Direction of Collision]	0	0	0		SH
	VTVSP0400/15D102222	Springfield	41.00	07/14/2015		[No Weather]		[No Direction of Collision]	0	0	0		SH
					08:14				0	0	0		SH
	VTVSP0400/15D102552	Springfield	41.00			[No Weather]		[No Direction of Collision]	-	-	Ű		
	VTVSP0400/15D103287	Springfield	41.00	10/24/2015		[No Weather]		[No Direction of Collision]	0	0	0		SH
	VTVSP0400/16D100312	Springfield	41.00	02/09/2016	08:01	[No Weather]	c10	[No Direction of Collision]	0	0	0		SH State Owned
	VTVSP1600/16D001283	Springfield	41.00	08/23/2016	22:55	[No Weather]	MISS	[No Direction of Collision]	0	0	0		SH State Owned
	VTVSP0400/12D100235	Springfield	41.17	01/18/2012	09:40	Clear	Failure to keep in proper lane, Operating vehicle in erratic, reckless, careless, negligent, or aggressive manner, No improper driving	Same Direction Sideswipe	0	0	0	N	SH
	VTVSP0400/12D102132	Springfield	41.35	07/10/2012	13:21	Cloudy	Failure to keep in proper lane	Single Vehicle Crash	0	0	0	S	SH
	VTVSP0400/13D104113	Springfield	41.35	12/29/2013	18:04	[No Weather]	VER	[No Direction of Collision]	0	0	0		SH
	VTVSP0400/13D104107	Springfield	41.50	12/29/2013	17:40	[No Weather]	0	[No Direction of Collision]	0	0	0		SH
	VTVSP0400/12D103963	Springfield	41.55	12/09/2012	08:02	Cloudy	Driving too fast for conditions	Single Vehicle Crash	0	0	0	S	SH
	VTVSP0400/14D101365	Springfield	41.55	05/08/2014	18:35	Clear	Distracted	Single Vehicle Crash	0	0	0	S	SH
	VTVSP1600/16D003100	Springfield	41.60	10/27/2016	21:58	Snow	Driving too fast for conditions, Failure to keep in proper lane	Other - Explain in Narrative	0	0	0	S	SH State Owned
	VTVSP0400/12D101006	Springfield	41.67	03/29/2012	17:40	Cloudy	Failure to keep in proper lane, Driving too fast for conditions	Single Vehicle Crash	1	0	0	Ν	SH
	VTVSP0400/12D102701	Springfield	41.70	08/23/2012	15:54	Clear	Made an improper turn, No improper driving	Same Direction Sideswipe	0	0	0	Ν	SH
	VTVSP0400/13D100244	Springfield	41.71	01/21/2013	19:46	Snow	Driving too fast for conditions	Single Vehicle Crash	0	0	0	Ν	SH
	VTVSP0400/13D104111	Springfield	41.72	12/29/2013	18:01	[No Weather]		[No Direction of Collision]	0	0	0		SH
	VTVSP0400/12D102315	Springfield	41.95	07/28/2012	14:47	Rain	Driving too fast for conditions	Single Vehicle Crash	0	0	0	Ν	SH
	VTVSP0400/13D100446	Springfield	42.00	02/11/2013	10:07	Snow	Driving too fast for conditions	Single Vehicle Crash	0	0	0	Ν	SH
	VTVSP0400/13D103779	Springfield	42.00	11/30/2013	14:11	[No Weather]		[No Direction of Collision]	0	0	0		SH
	VTVSP0400/14D100897	Springfield	42.00	03/20/2014	16:09	[No Weather]		[No Direction of Collision]	0	0	0		SH
	VTVSP0400/15D100345	Springfield	42.00	02/02/2015	10:15	Snow	Driving too fast for conditions, Followed too closely, No improper driving	Rear End	1	0	0	S	SH
	VTVSP0400/15D102152	Springfield	42.00	07/08/2015	10:03	[No Weather]		[No Direction of Collision]	0	0	0		SH
	VTVSP0400/15D103859	Springfield	42.00	12/29/2015	10:18	[No Weather]		[No Direction of Collision]	0	0	0		SH

*Crash occurred prior to the last Highway Improvement Project. This data should not be used in a crash analysis. UNK indicates Mile Marker is Unknown.

Vermont Agency of Transportation

Statewide Sections - Route Log Order /2 - Statewide

Years: 2010 - 2014

H.C.L No.	/3. Route	System	Town	Mileage	ADT	Years C	rashes Fa	atalities Ir	ijuries c	PDO Crashes	Critical Rate	Actual Rate	Ratio Actual/Critical	Severity Index (\$/Accident/1.)
	503 I-91	Interstate, Rural (r)	Vernon, Guilford	5.000 - 5.300	16700	5	12	0	1	11	1.168	1.312	1.124	\$14,733
	504 I-91	Interstate, Rural (r)	Guilford	6.000 - 6.300	16700	5	12	0	1	11	1.168	1.312	1.124	\$14,733
	521 I-91	Interstate, Urban (r)	Brattleboro	7.600 - 7.900	18900	5	11	0	1	10	0.967	1.063	1.099	\$15,264
	290 I-91	Interstate, Urban (r)	Brattleboro	8.500 - 8.800	18900	5	14	0	4	11	0.967	1.352	1.399	\$29,536
	111 I-91	Interstate, Urban (r)	Brattleboro	9.000 - 9.300	22774	5	22	0	5	17	0.926	1.764	1.904	\$24,809
	505 I-91	Interstate, Urban (r)	Brattleboro	9.800 - 10.100	22800	5	13	0	0	13	0.926	1.041	1.124	\$8,900
	394 I-91	Interstate, Rural (r)	Dummerston	17.800 - 18.100	14600	5	12	0	5	9	1.205	1.501	1.246	\$39,550
	530 I-91	Interstate, Rural (r)	Putney	18.400 - 18.700	10200	5	8	0	1	7	1.314	1.432	1.09	\$17,650
	310 I-91	Interstate, Rural (r)	Putney	19.000 - 19.300	10200	5	10	0	1	9	1.314	1.79	1.363	\$15,900
	417 I-91	Interstate, Rural (r)	Putney	19.600 - 19.900	10200	5	9	0	1	8	1.314	1.611	1.226	\$16,678
	308 I-91	Interstate, Rural (r)	Putney	21.000 - 21.300	10200	5	10	0	4	7	1.314	1.79	1.363	\$37,790
	415 I-91	Interstate, Rural (r)	Westminster	24.000 - 24.300	10200	5	9	0	4	7	1.314	1.611	1.226	\$41,989
	186 I-91	Interstate, Rural (r)	Westminster, Rockingham	31.000 - 31.300	12400	5	14	0	7	10	1.253	2.062	1.646	\$45,807
	620 I-91	Interstate, Rural (r)	Rockingham	35.000 - 35.300	11155	5	8	0	1	7	1.285	1.309	1.019	\$17,650
	276 I-91	Interstate, Rural (r)	Rockingham	36.400 - 36.700	10900	5	11	0	5	7	1.292	1.843	1.426	\$41,527
	277 I-91	Interstate, Rural (r)	Rockingham	37.900 - 38.200	10900	5	11	0	0	11	1.292	1.843	1.426	\$8,900
	458 I-91	Interstate, Rural (r)	Rockingham, Springfield	39.000 - 39.300	10900	5	9	0	3	7	1.292	1.508	1.166	\$33,222
	457 l-91	Interstate, Rural (r)	Springfield	40.000 - 40.300	10900	5	9	0	5	6	1.292	1.508	1.166	\$49,767
	76 I-91	Interstate, Rural (r)	Springfield	40.800 - 41.100	10900	5	16	0	2	14	1.292	2.681	2.074	\$17,650
	266 I-91	Interstate, Rural (r)	Springfield	41.500 - 41.800	10650	5	11	0	2	9	1.3	1.886	1.451	\$21,627
	416 I-91	Interstate, Rural (r)	Springfield	42.100 - 42.400	10200	5	9	0	3	6	1.314	1.611	1.226	\$32,233
	414 I-91	Interstate, Rural (r)	Springfield	43.000 - 43.300	10200	5	9	0	5	5	1.314	1.611	1.226	\$48,778

Appendix N: Detour Routes

This option would close the section of I-91 between the on and off ramps at exit 7.

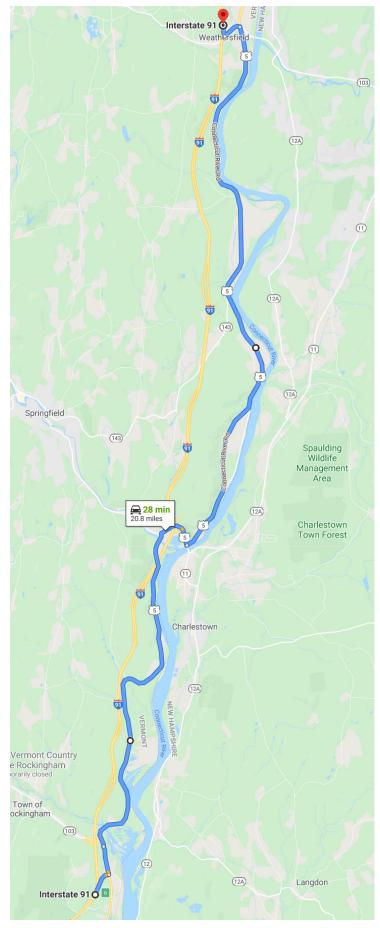
I-91 Northbound: Traffic traveling northbound on I-91, would utilize US Route 5 between exit 6 and exit 8. The through distance on the US Route 5 detour is almost identical at 20.8 miles versus the 17.7 miles on I-91, with travel times estimated at 28 minutes for the detour route and 19 minutes for traveling on I-91.

I-91 Southbound: The detour would utilize the on and off ramps at exit 7 for southbound traffic. This detour would not add any distance to the through route.

It is recommended that a detour only be utilized for brief closure periods during off peak hours, such as nights or weekends, in order to rapidly replace the deck or superstructures. The methods available to replace a deck or superstructure during a short closure period include: lateral slide, self-propelled modular transporters (SPMTs), and prefabricated bridge elements.

I-91 Northbound Detour:

Traffic traveling northbound on I-91, would utilize US Route 5 between exit 6 and exit 8. The through distance on the US Route 5 detour is almost identical at 20.8 miles versus the 17.7 miles on I-91, with travel times estimated at 28 minutes for the detour route and 19 minutes for traveling on I-91.

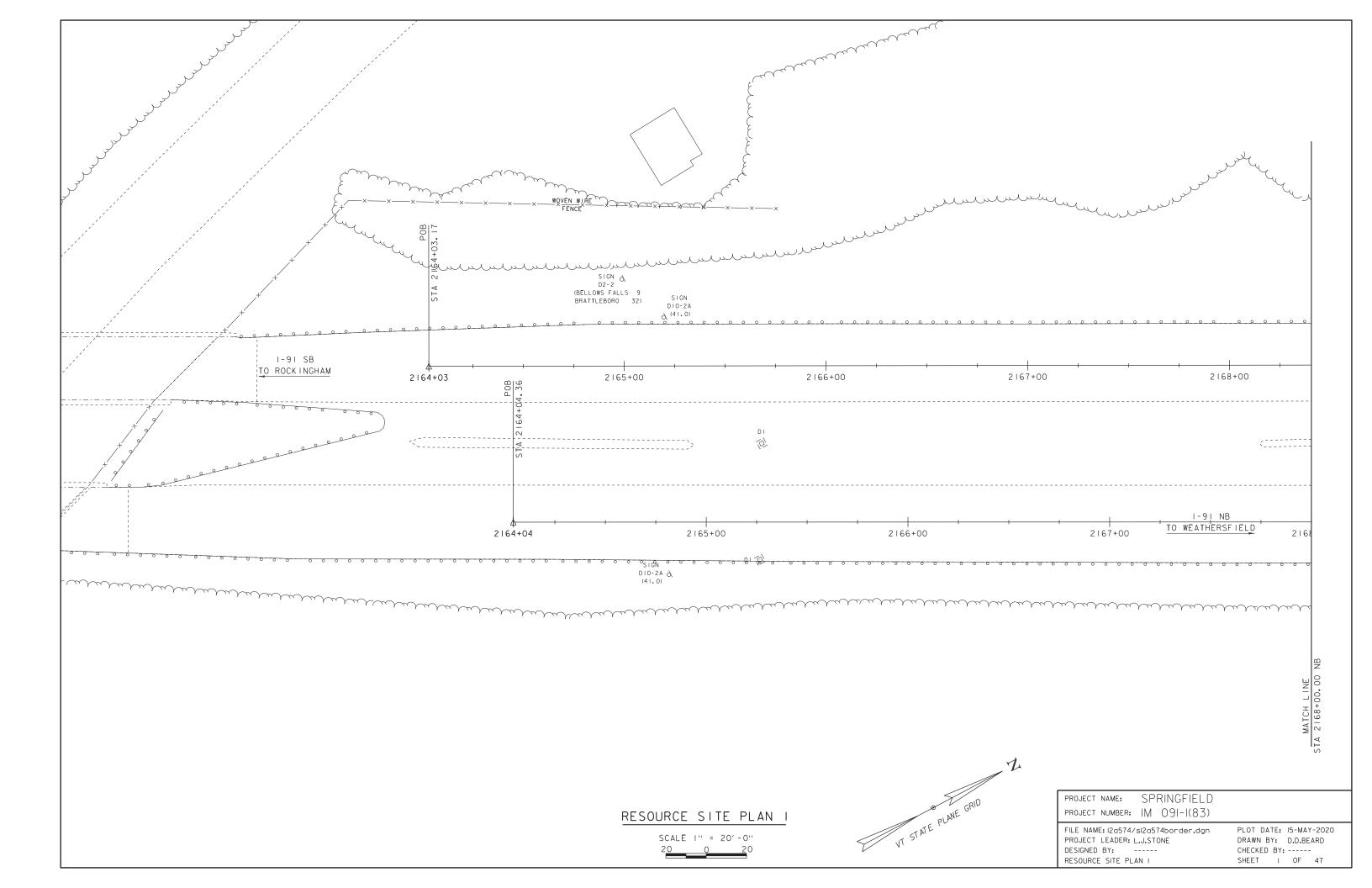


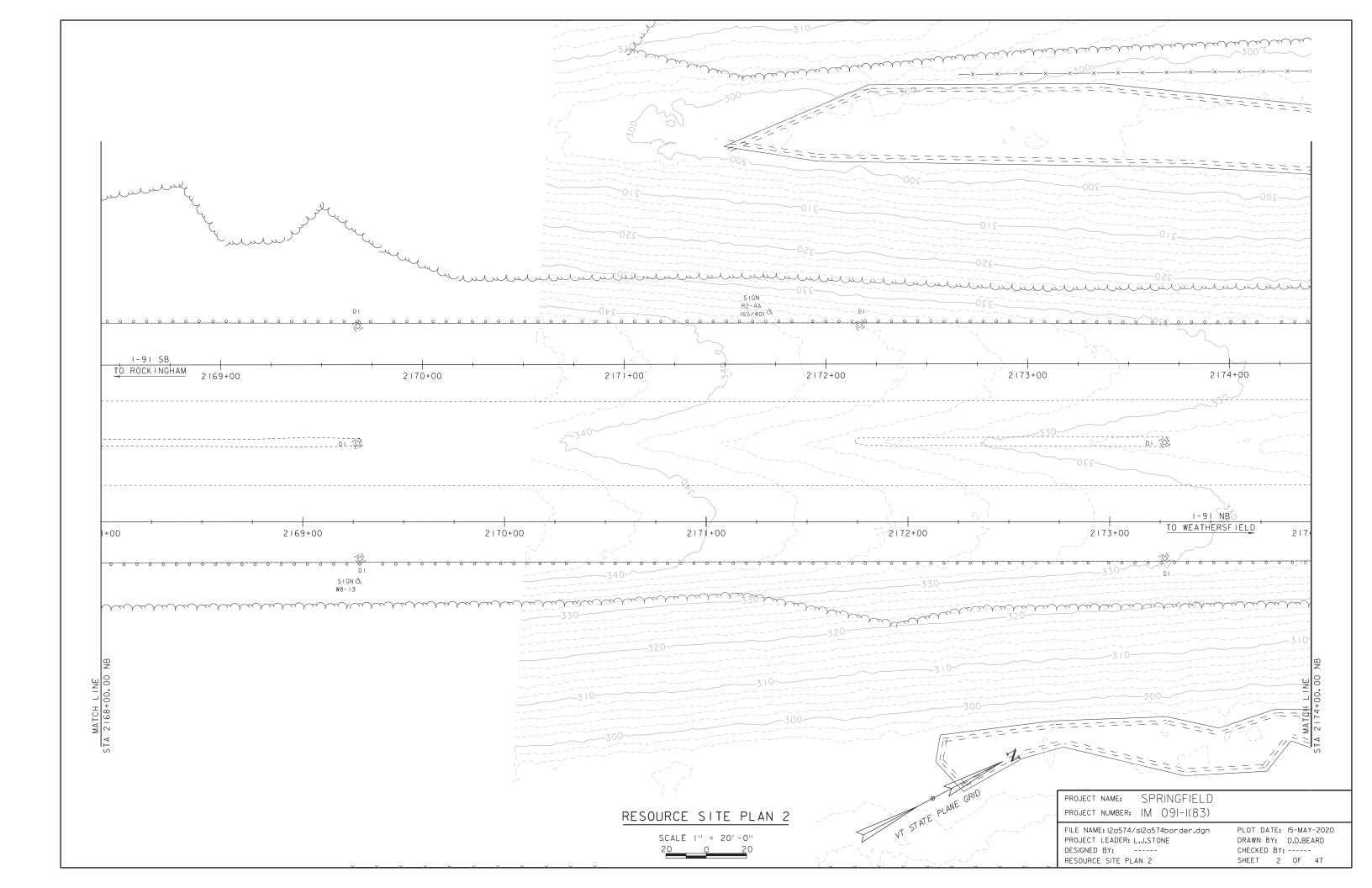
I-91 Southbound Detour:

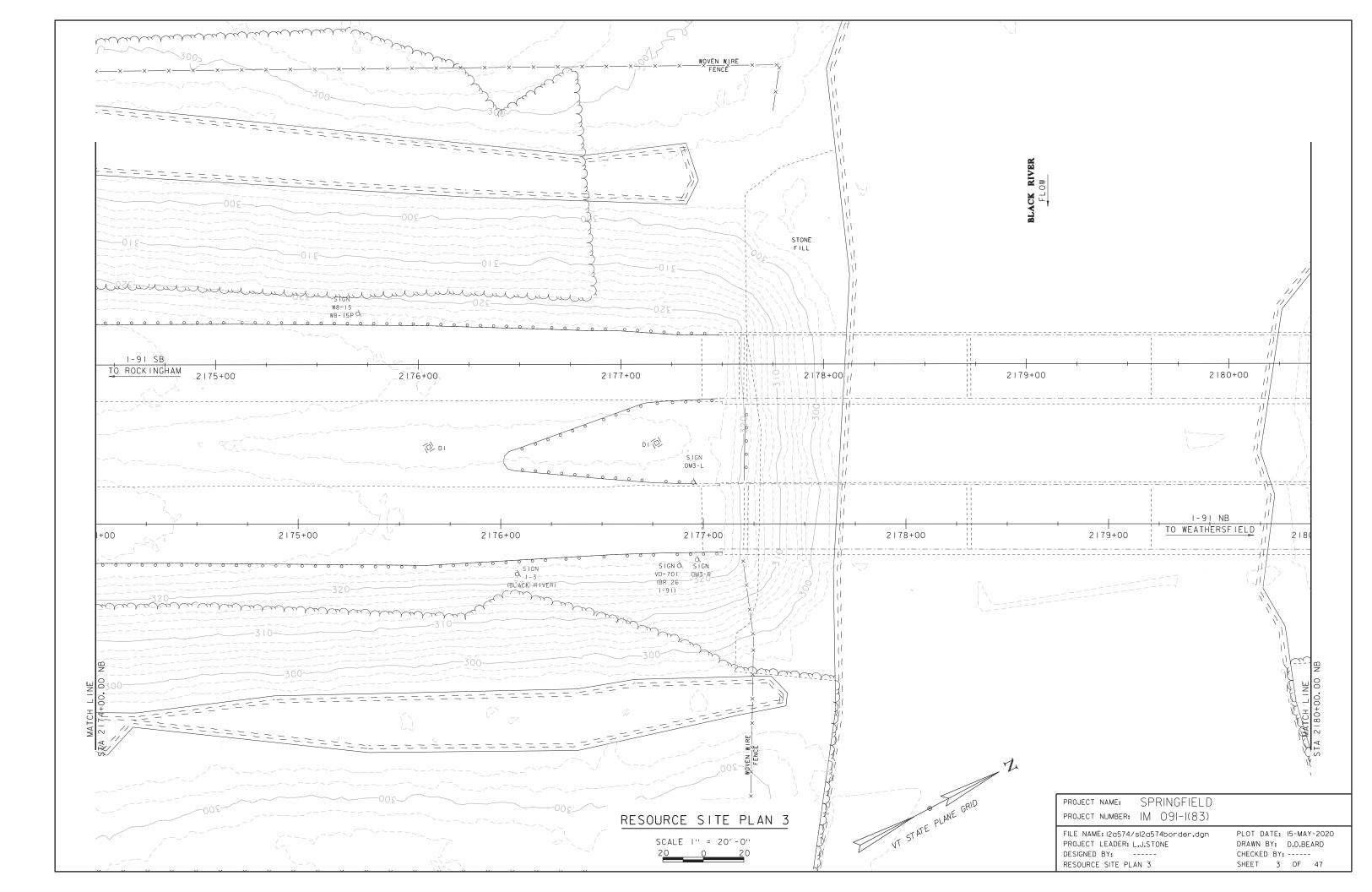
Traffic traveling Southbound on I-91, would utilize the on and off ramps at exit 7 for southbound traffic. This detour would not add any distance to the through route. The median between US Route 5 northbound and southbound would need to be modified to allow traffic to cross over Route 5 during construction.

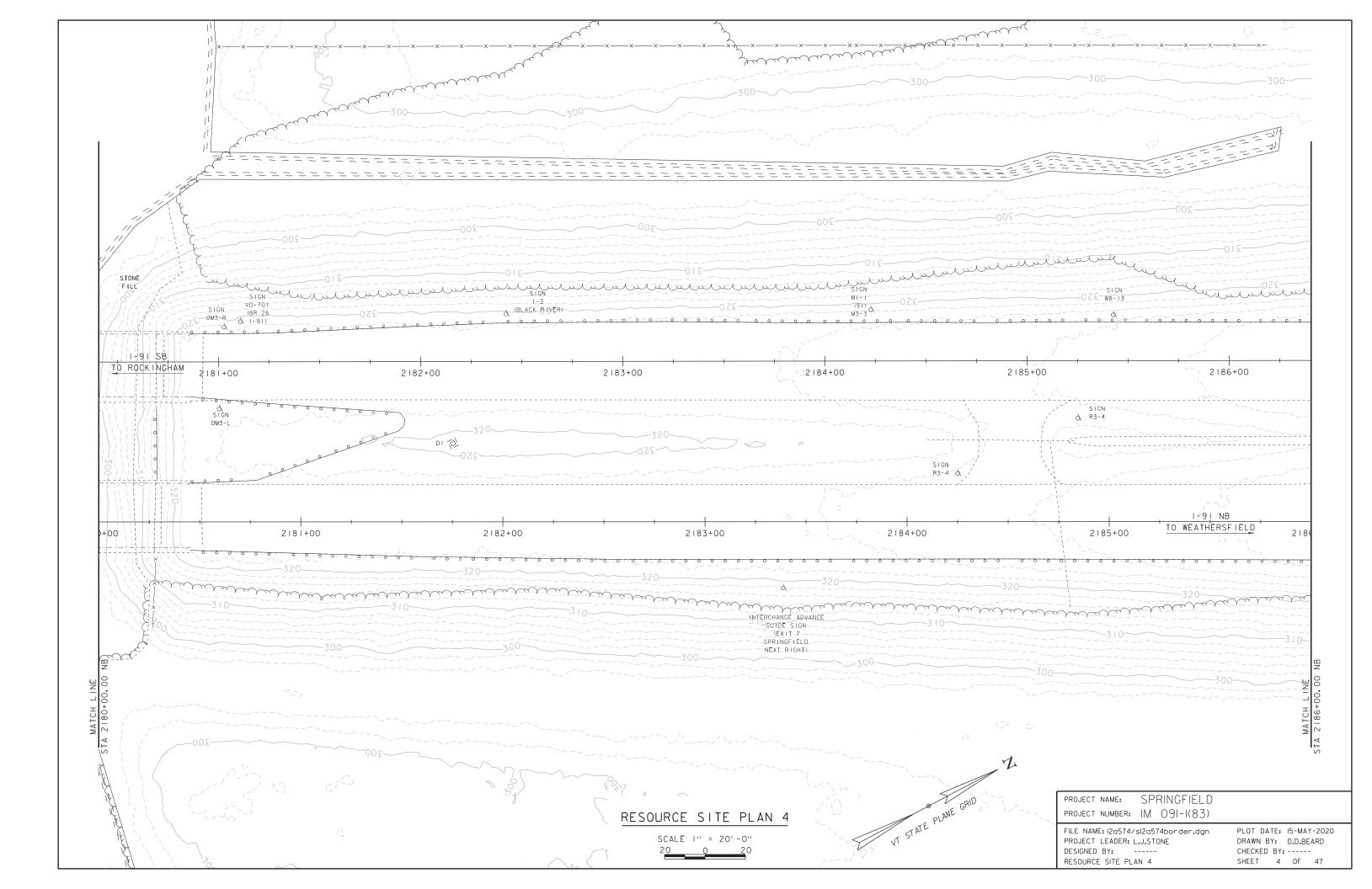


Appendix O: Plans

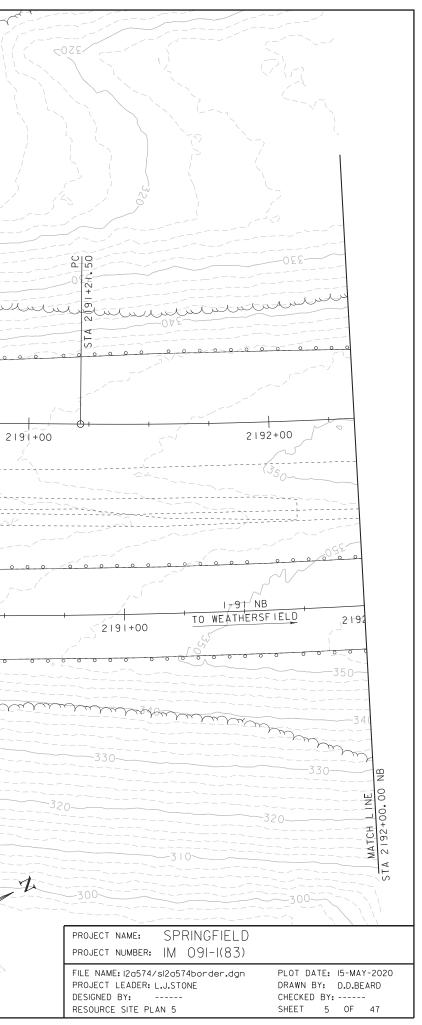


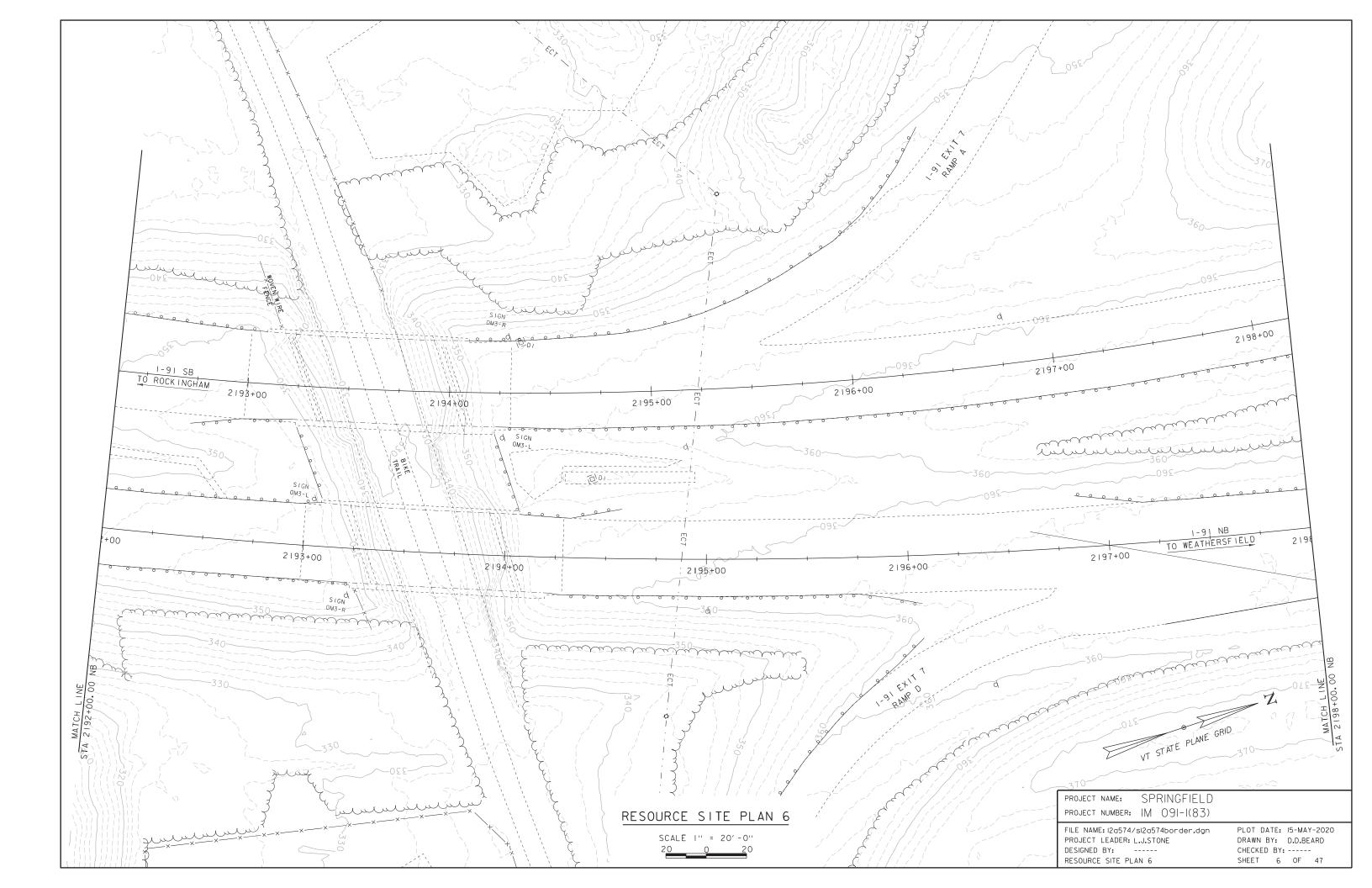


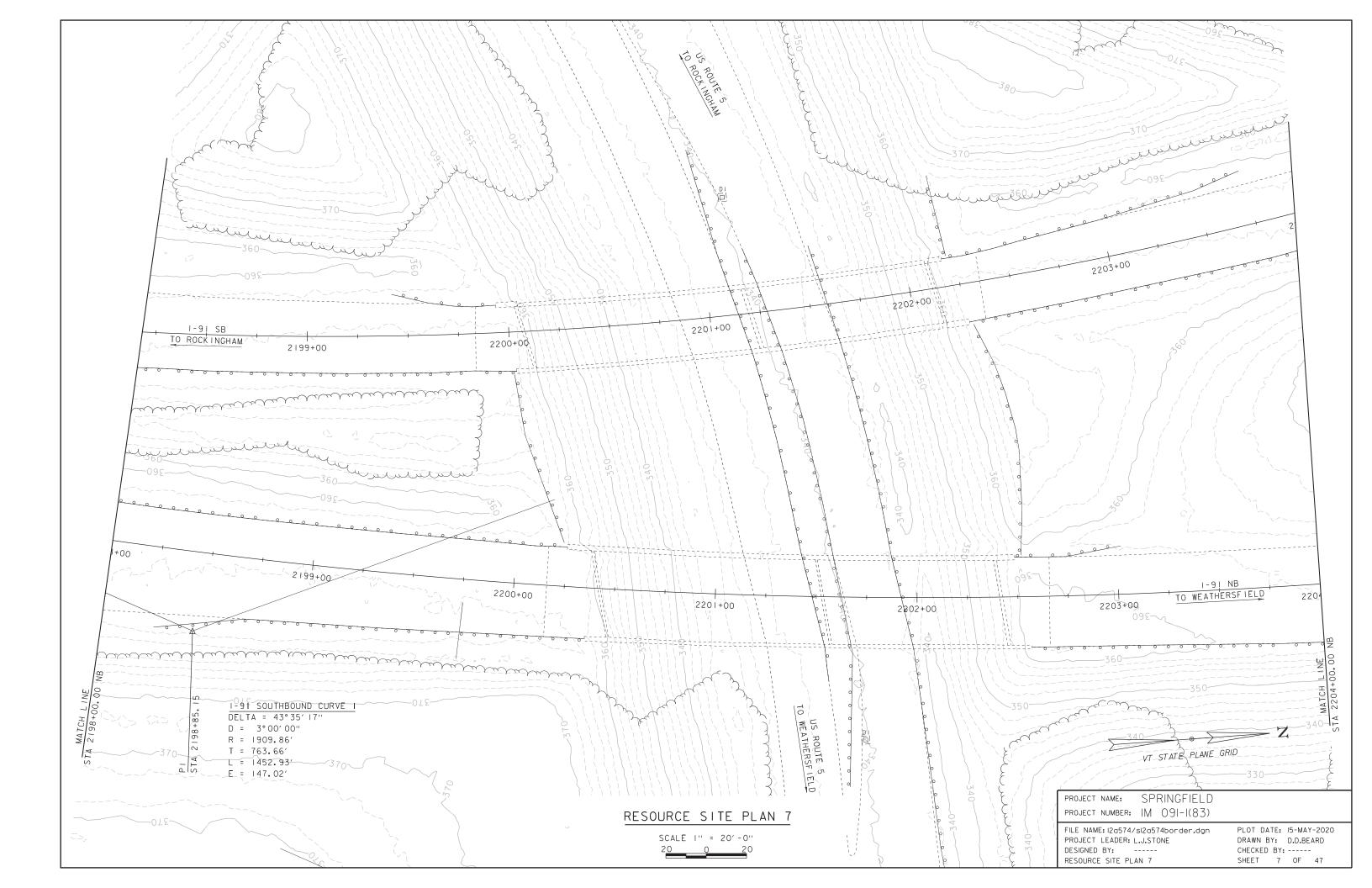


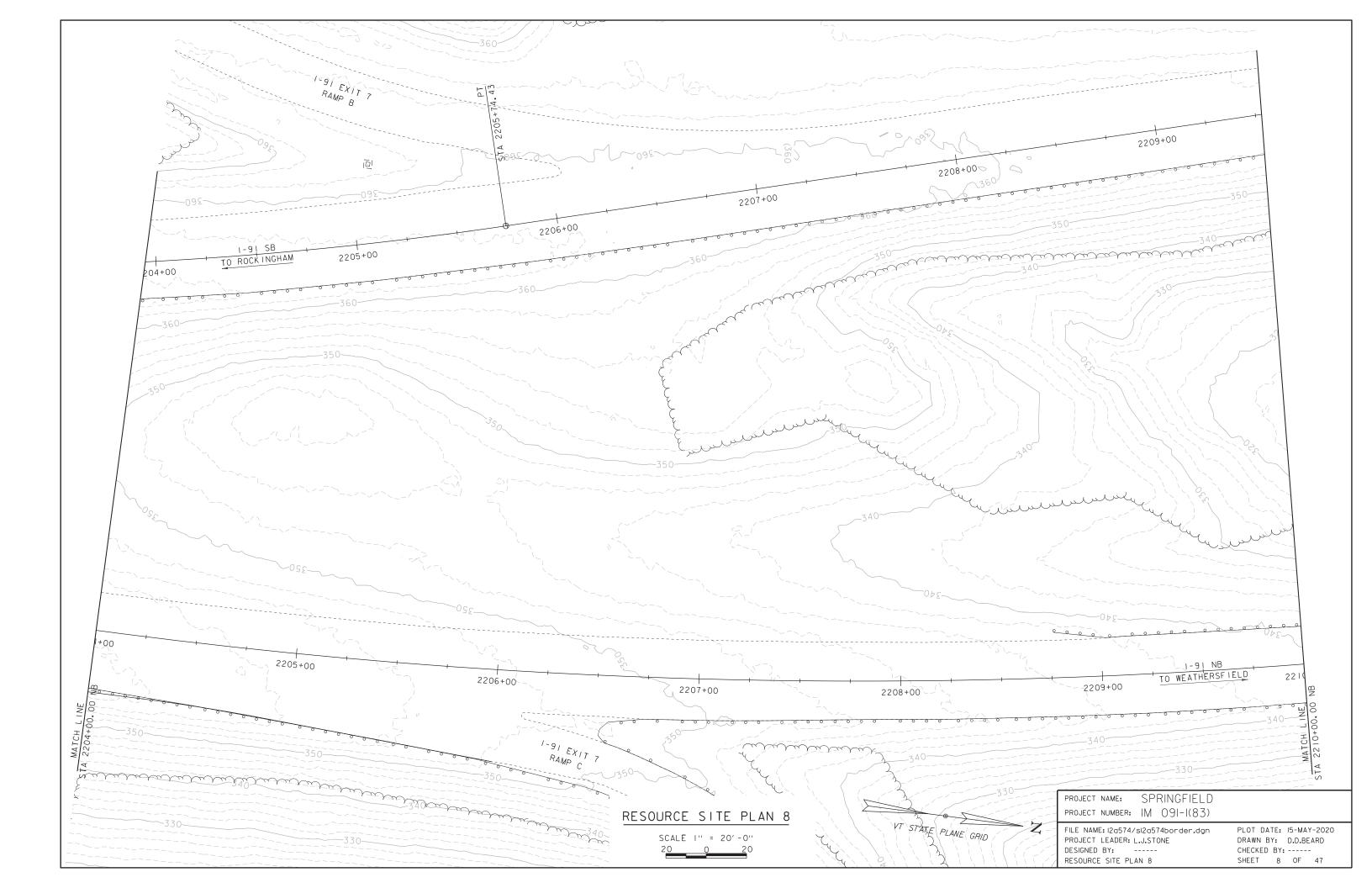


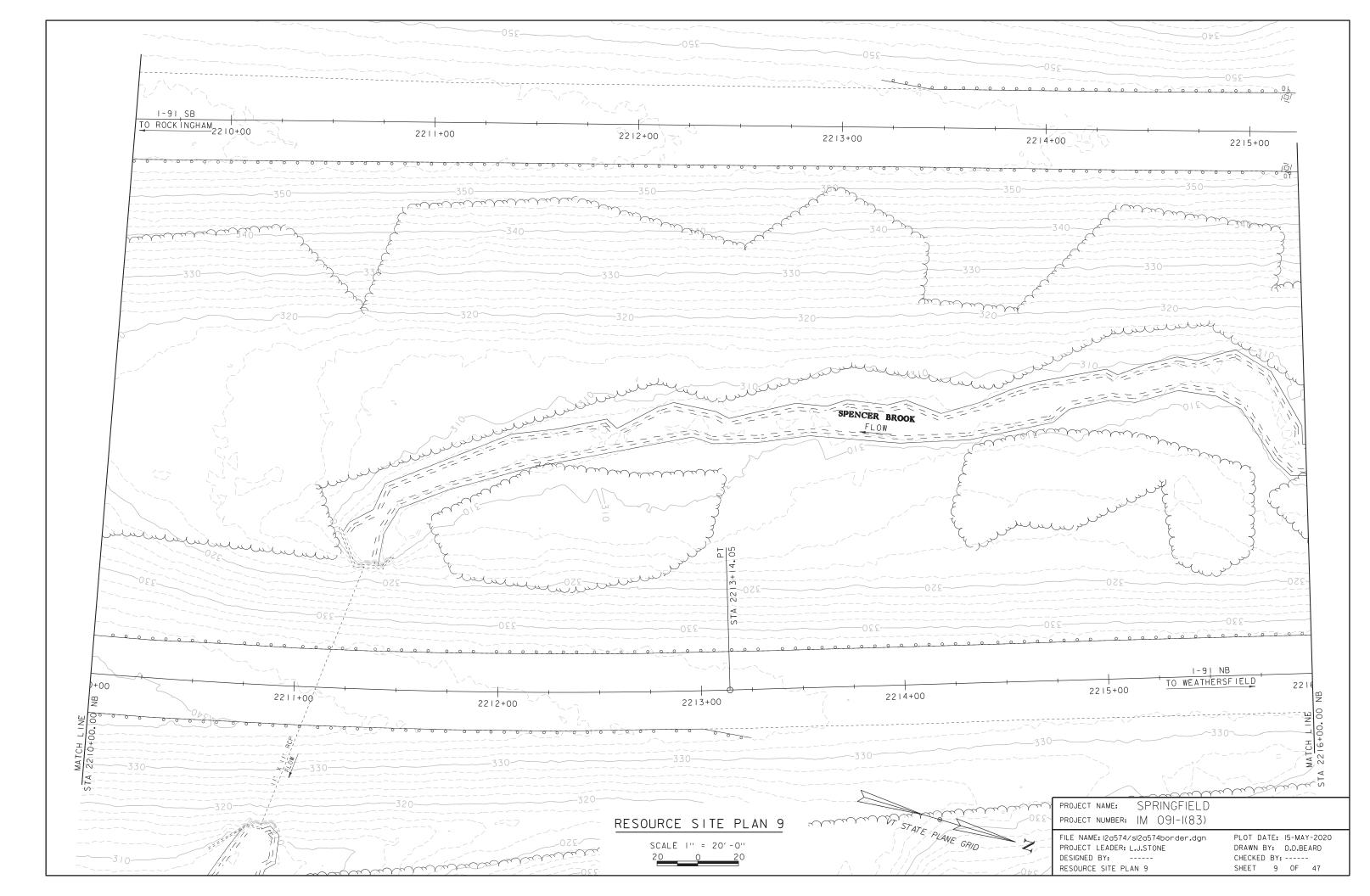
1-91 SB TO ROCK INGHAM 2187+00 2188+00 2189+00 2190+00 88 88 +00 2187+00 2188+00 2189+00 2190+00 \sim MATCH LINE STA 2186+00.00 VT STATE PLANE GRID RESOURCE SITE PLAN 5 SCALE I" = 20'-0" 20

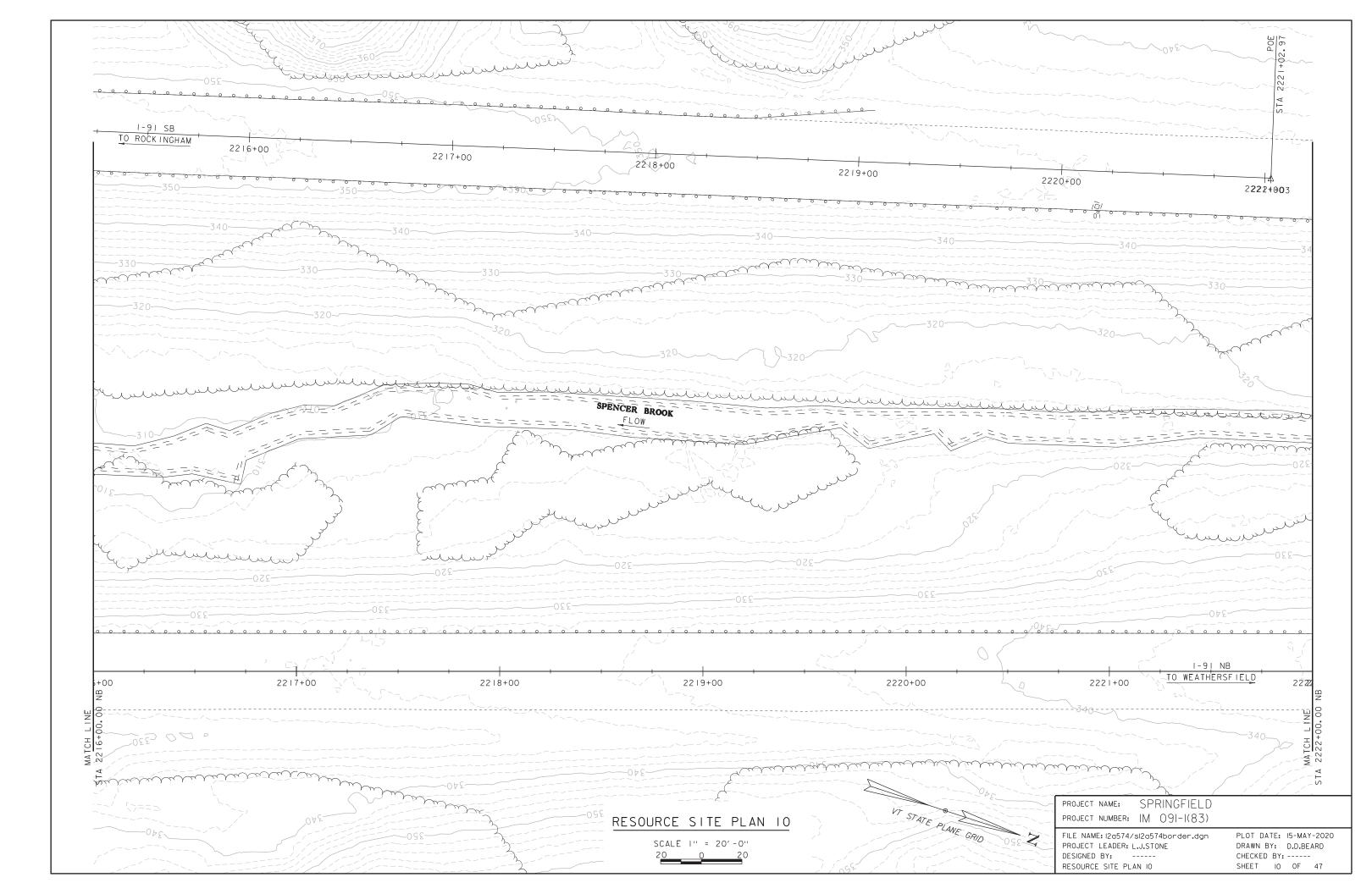


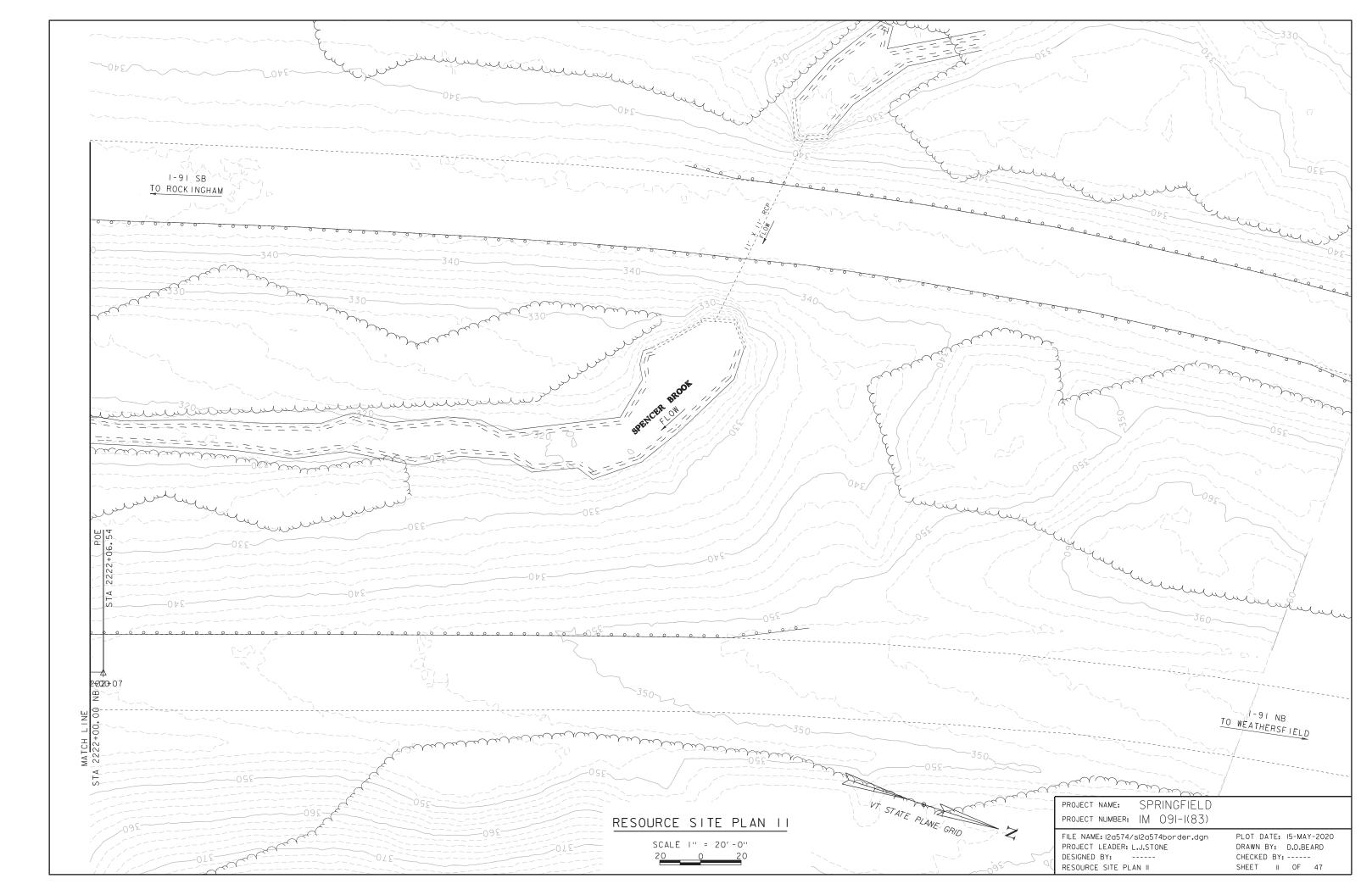




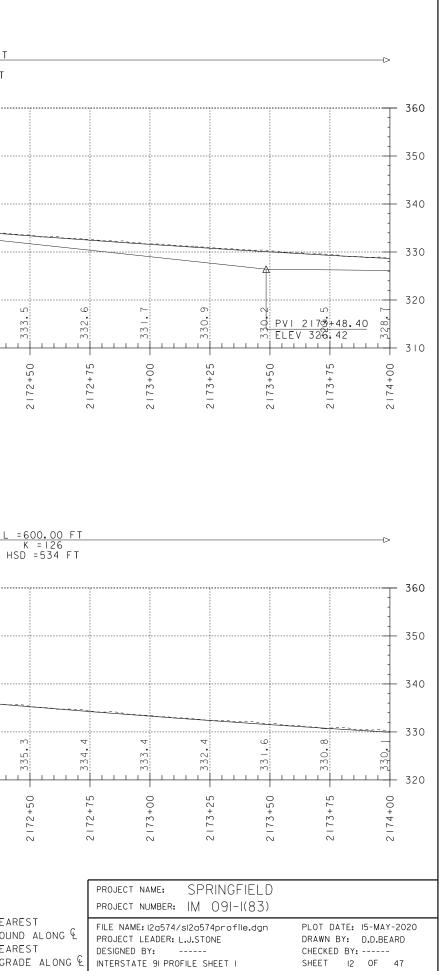


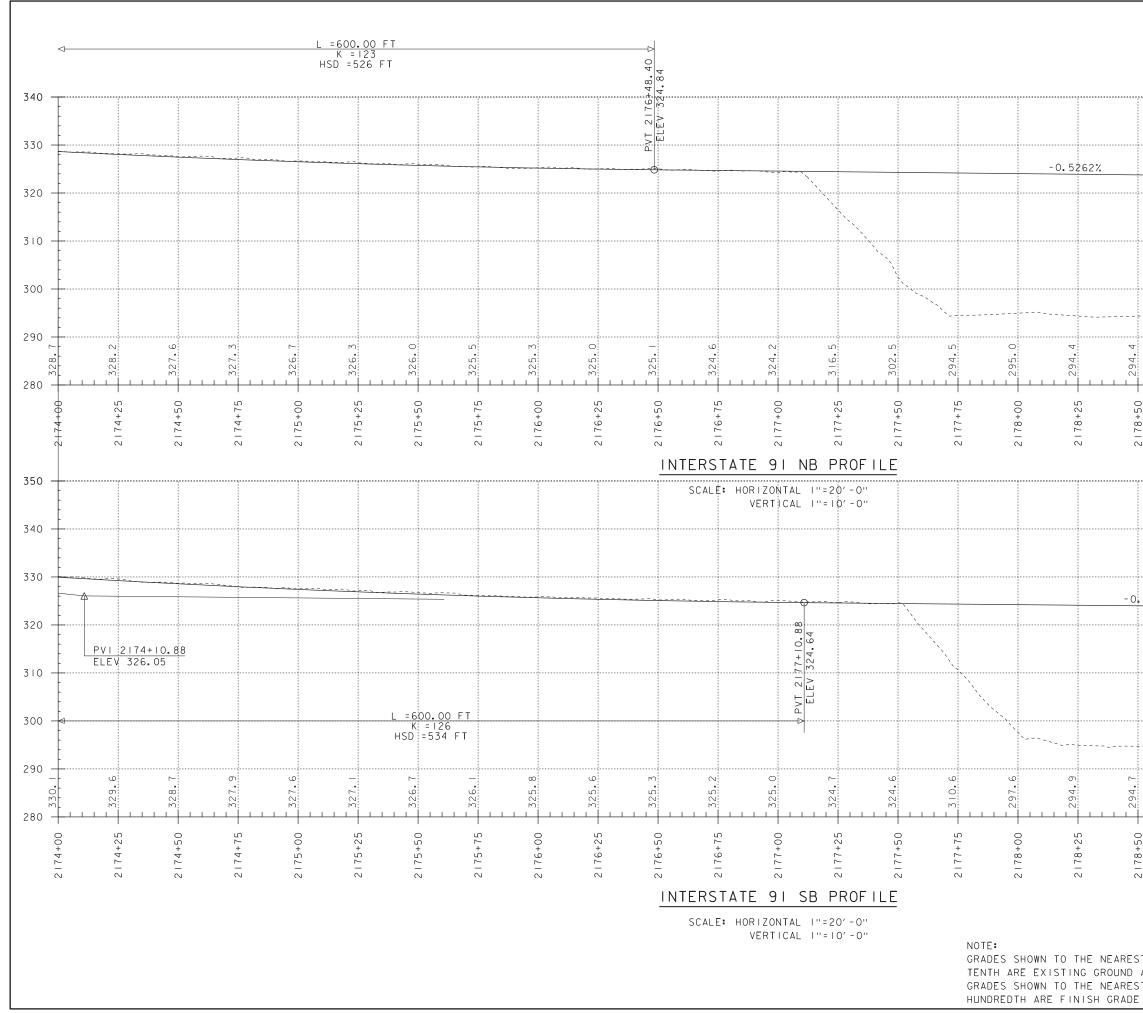




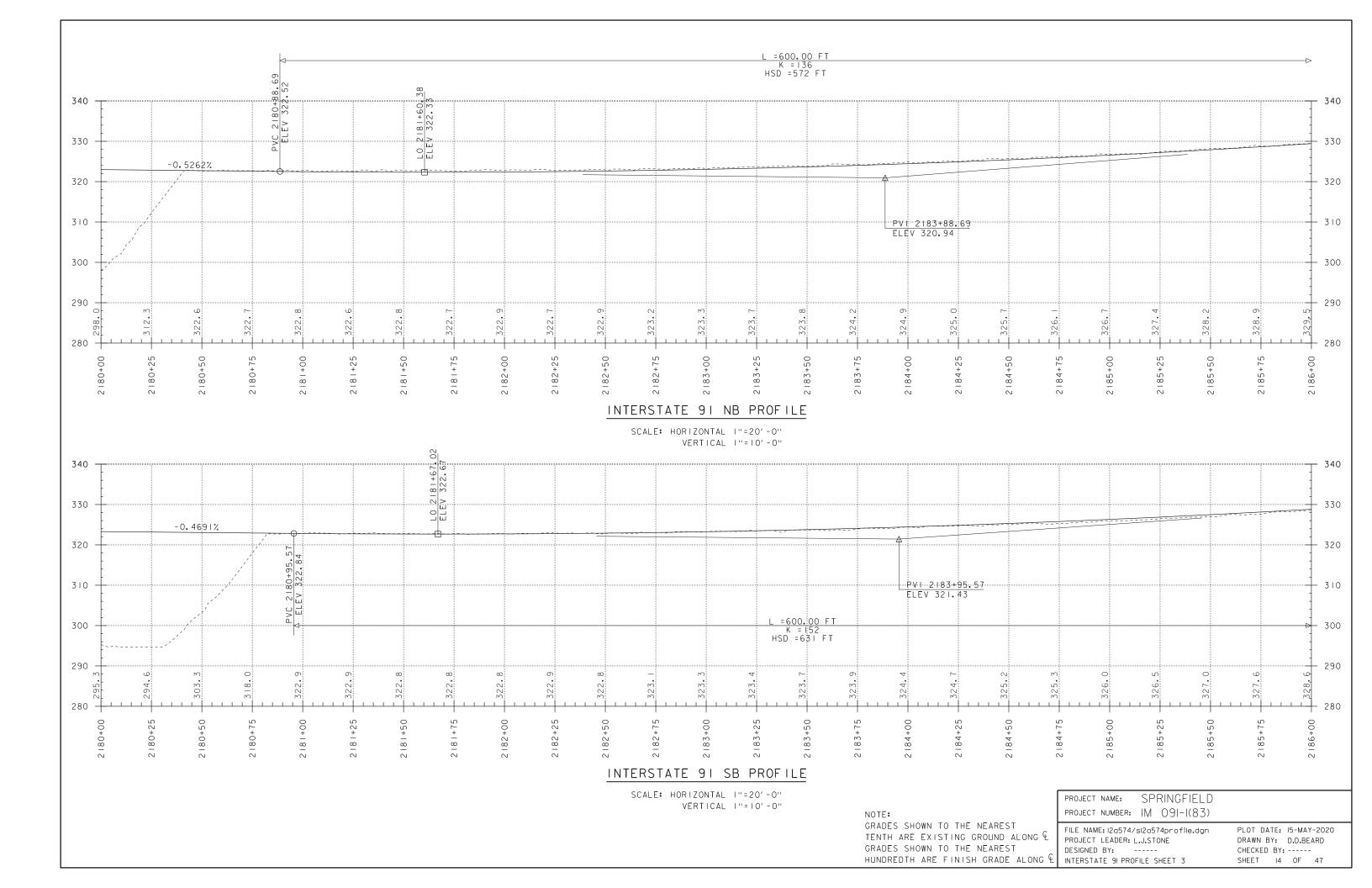


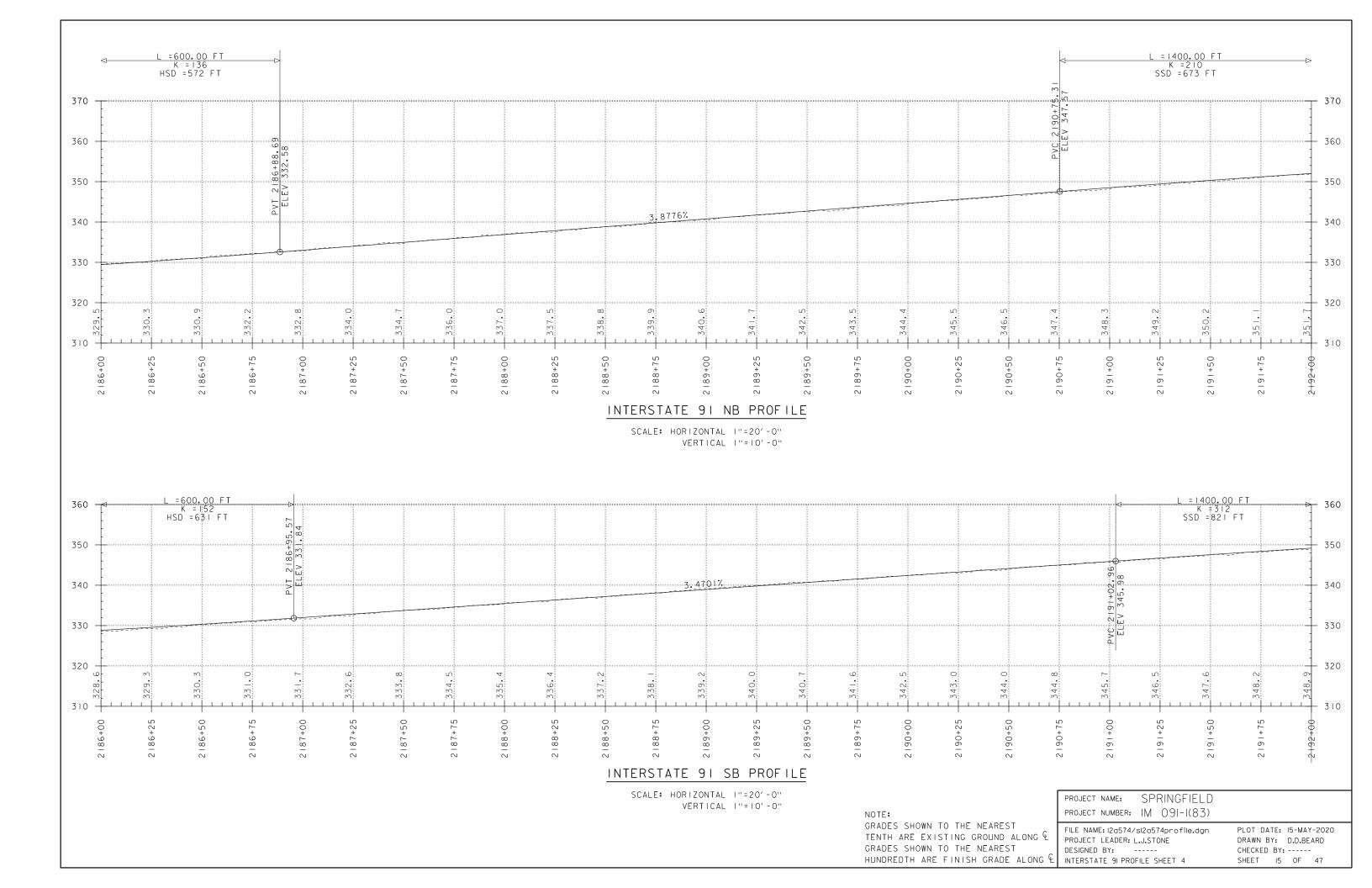
L = 600.00 FT K = 123 HSD = 526 FT PVC 2170+48.40 360 PVI 2170+11.48 ELEV 344.56 350 -5.3850% 340 330 320 ω 4 0 ω 9 \sim Q S 4 40. 39. 336. 334. 42. 335. 333. 4 310 -2170+25 2172+25 2169+25 2169+75 170+50 1+75 172+00 168+50 2170+00 70+75 00+ +50 00 +25 2168+75 00+ 2169+50 +25 2168+ +69 I l 68. 2171 ~ \sim 2 \sim \sim \sim \sim \sim \sim \sim \sim \sim INTERSTATE 91 NB PROFILE SCALE: HORIZONTAL I"=20'-0" VERTICAL I"= IO' - O" 10.88 360 2171+ PVI 2170+55.83 ELEV 344.65 PVC 350 -5.2386% 340 330 σ ω M \sim 4 m 43. 9. 0 E 338 42 36. 35 7 320 -2171+50 2171+75 2168+50 2169+00 2169+25 2169+50 2169+75 2170+00 2170+25 2170+50 2172+25 75 00+ +25 00+ 00-2168+25 2168+75 2170+. 2172+ l 68. 217 2171 \sim INTERSTATE 91 SB PROFILE SCALE: HORIZONTAL I"=20'-0" VERTICAL I"= 10' - 0" NOTE: GRADES SHOWN TO THE NEAREST TENTH ARE EXISTING GROUND ALONG € GRADES SHOWN TO THE NEAREST HUNDREDTH ARE FINISH GRADE ALONG €

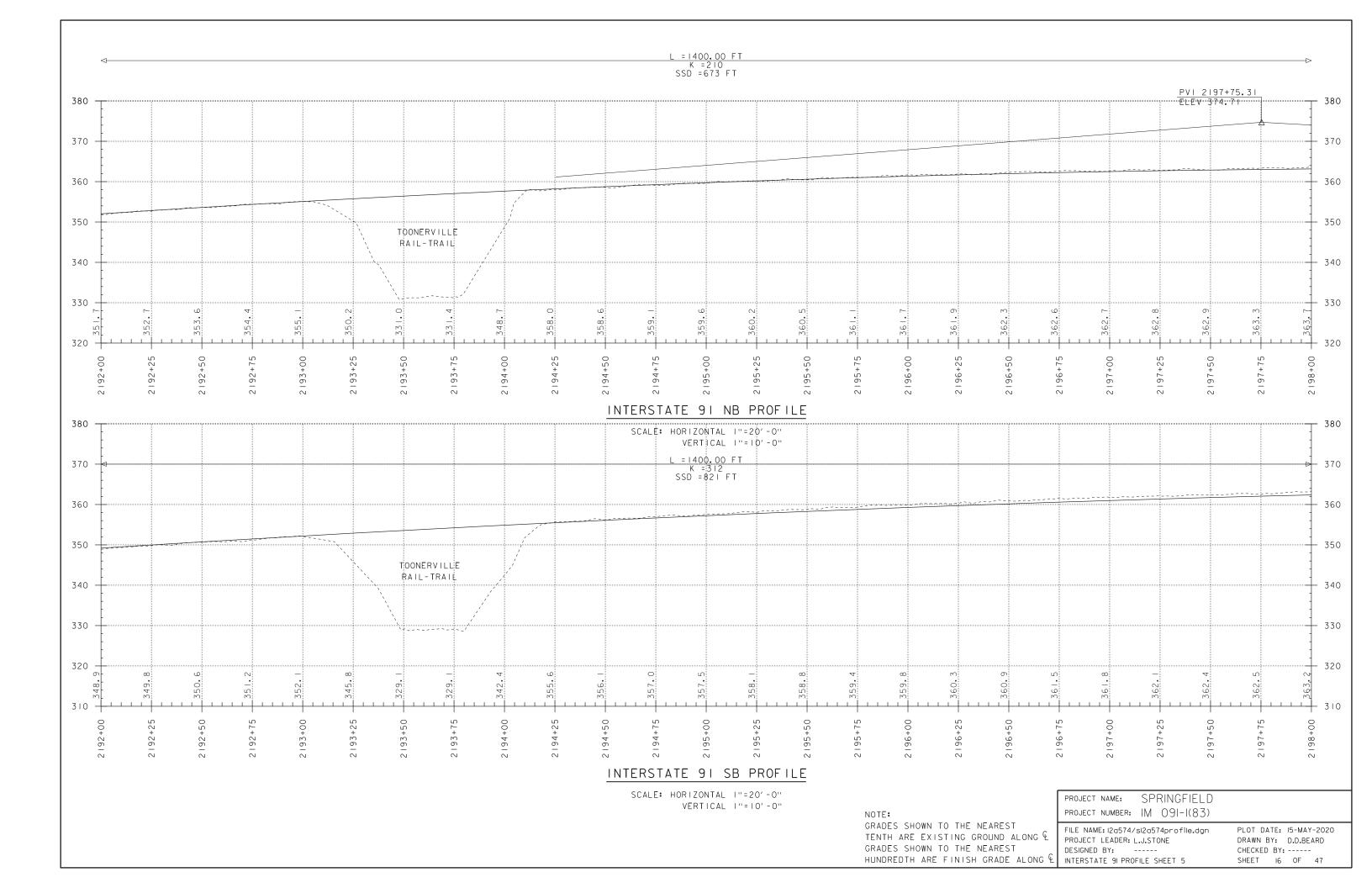


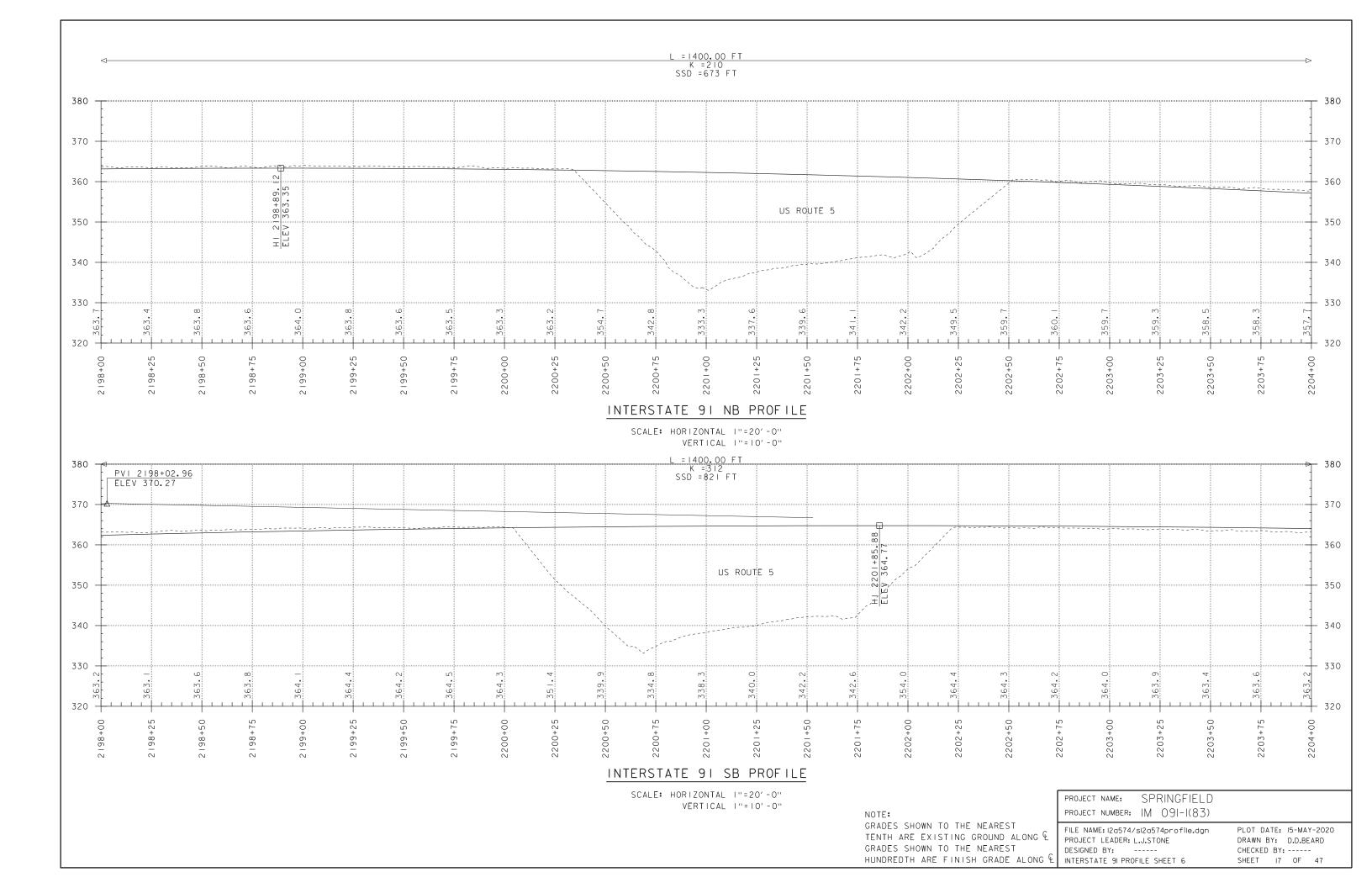


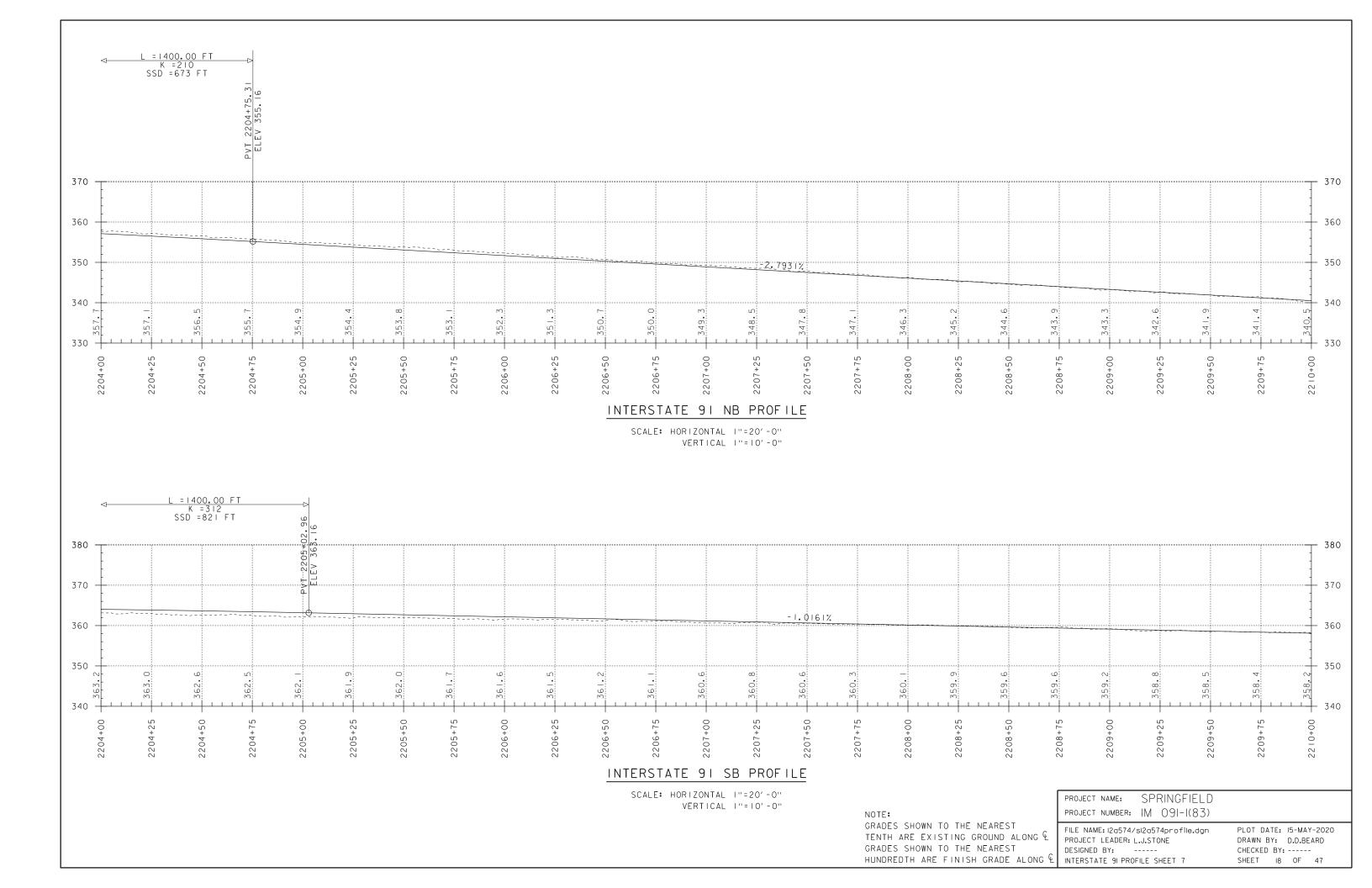
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ST ALONG & ST E ALONG &	PROJECT LEA DESIGNED BY	a574/sl2a574 NDER: L.J.STON 91 PROFILE SH	ΝE	DRAWN B	ATE: I5-MAY-2020 3Y: D.D.BEARD BY: I3 OF 47)

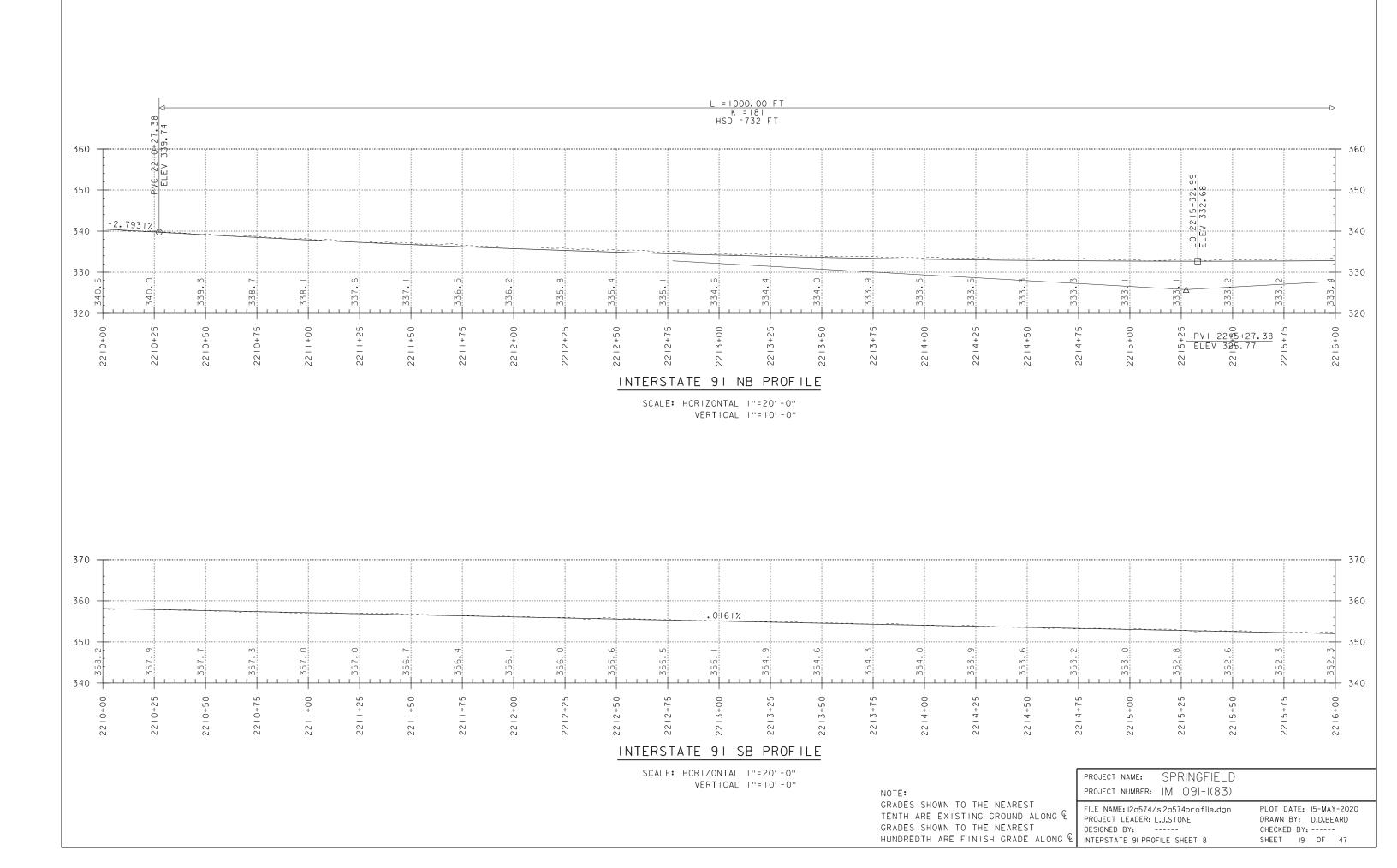


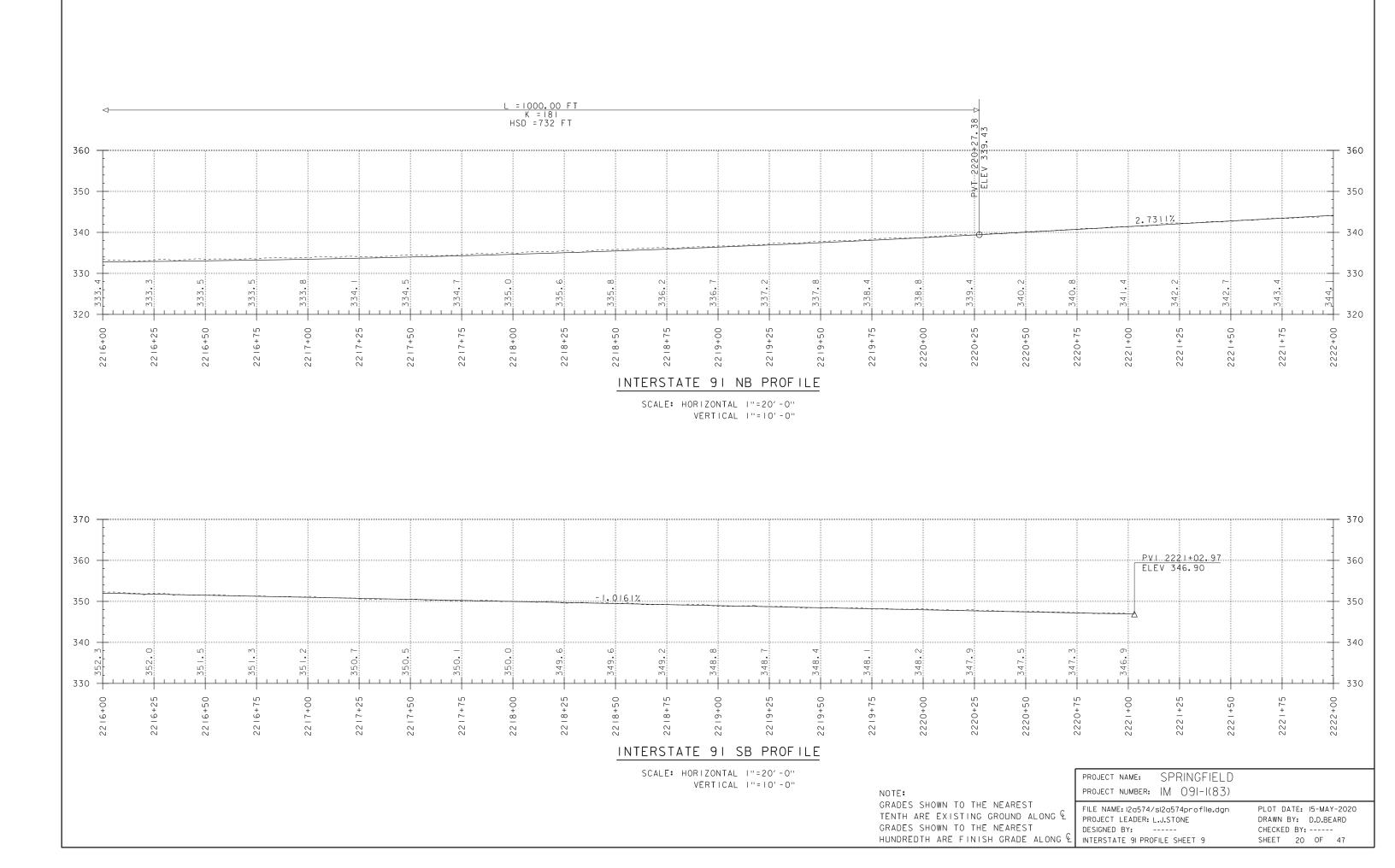


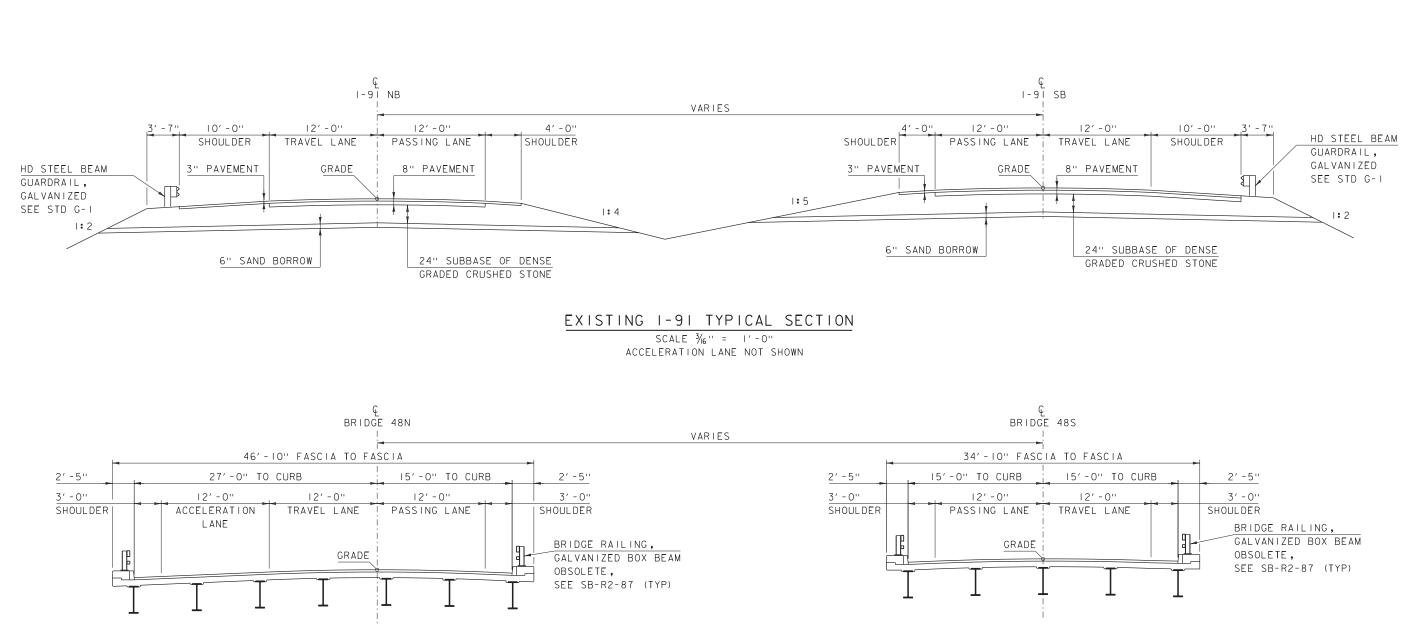








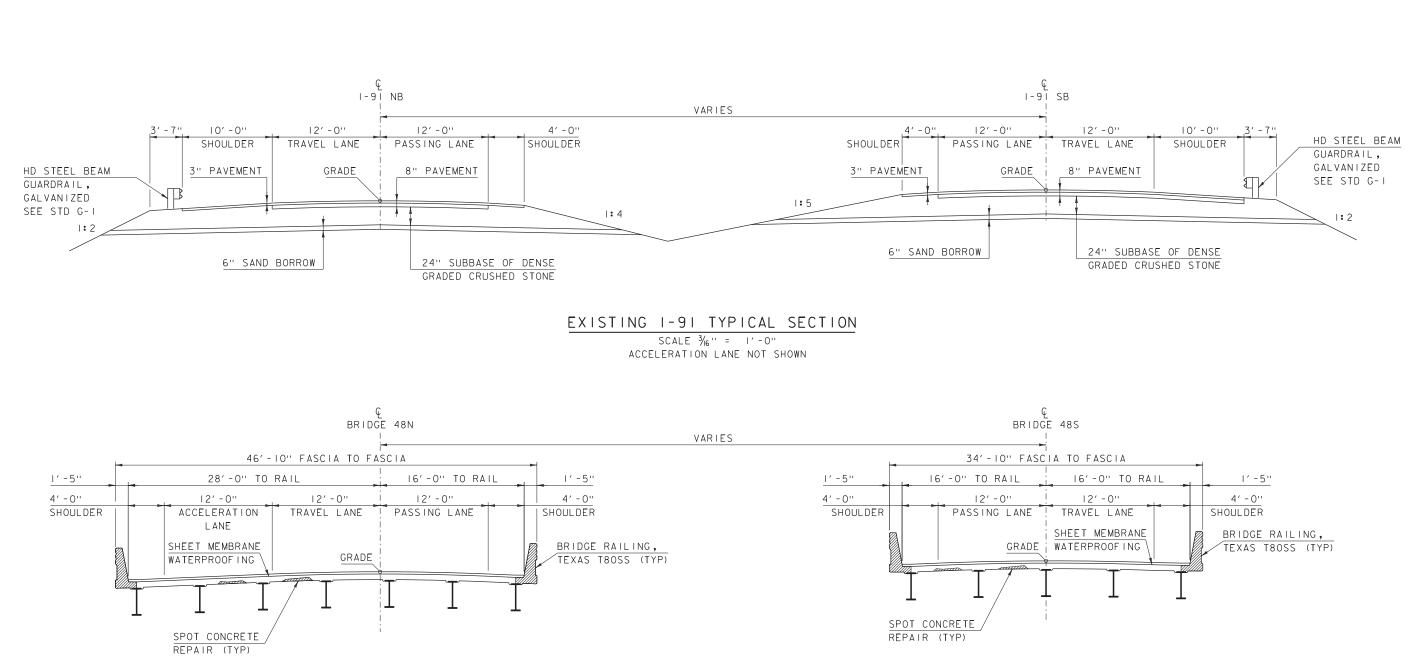




EXISTING BRIDGE 48 N/S TYPICAL SECTION

SCALE 3/16" = 1'-0" ALL DIMENSIONS ARE RADIAL UNLESS OTHERWISE NOTED

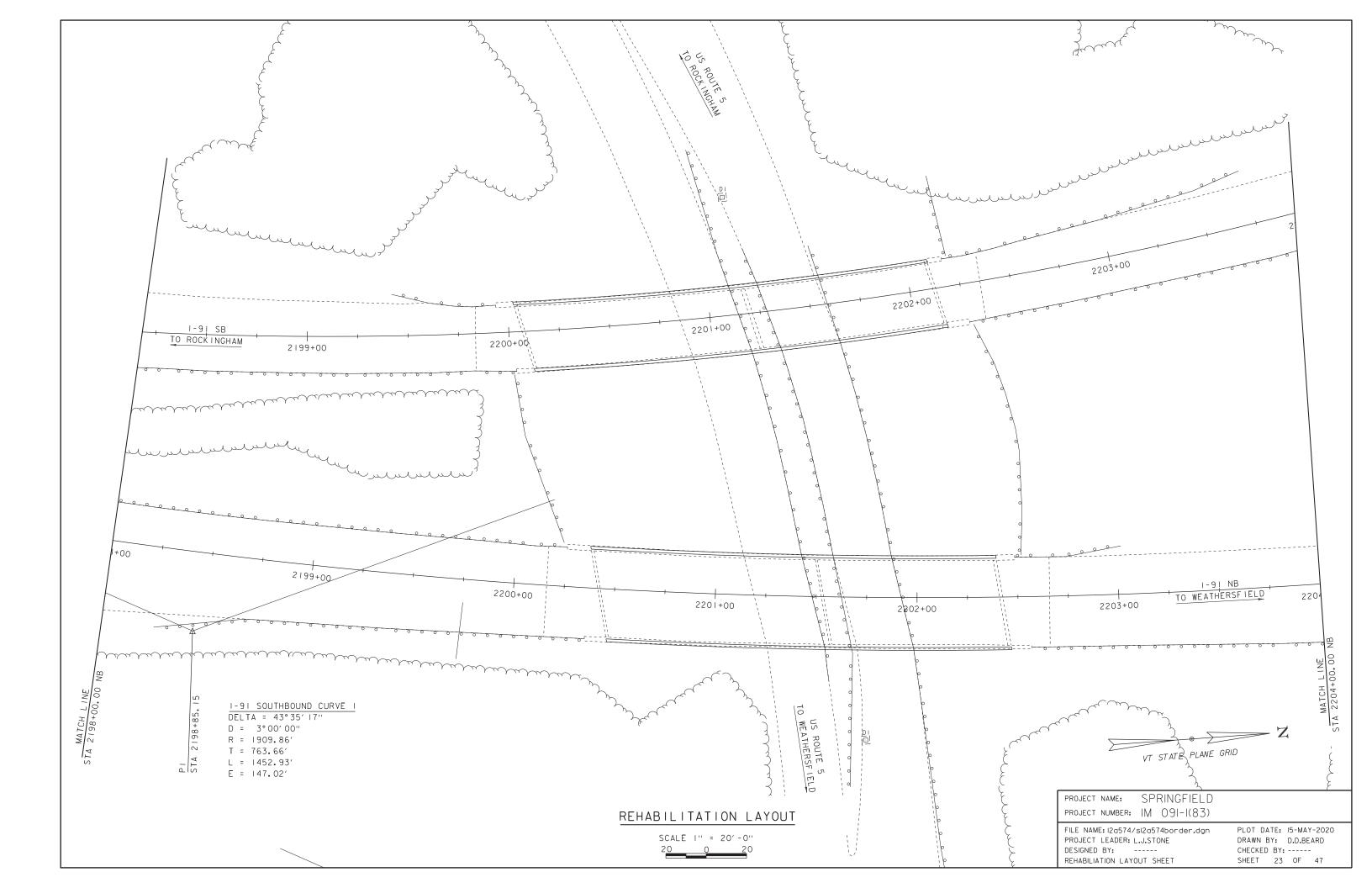
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PROJECT NUMBER:	IM 091-1(83)					
FILE NAME: 12a574/	sl2a574typ.dgn	PLOT DATE: 15-MAY-2020				
PROJECT LEADER:	.J.STONE	DRAWN BY: D.D.BEARD				
DESIGNED BY:		CHECKED BY:				
EXISTING TYPICAL S	SECTIONS	SHEET 21 OF 47				

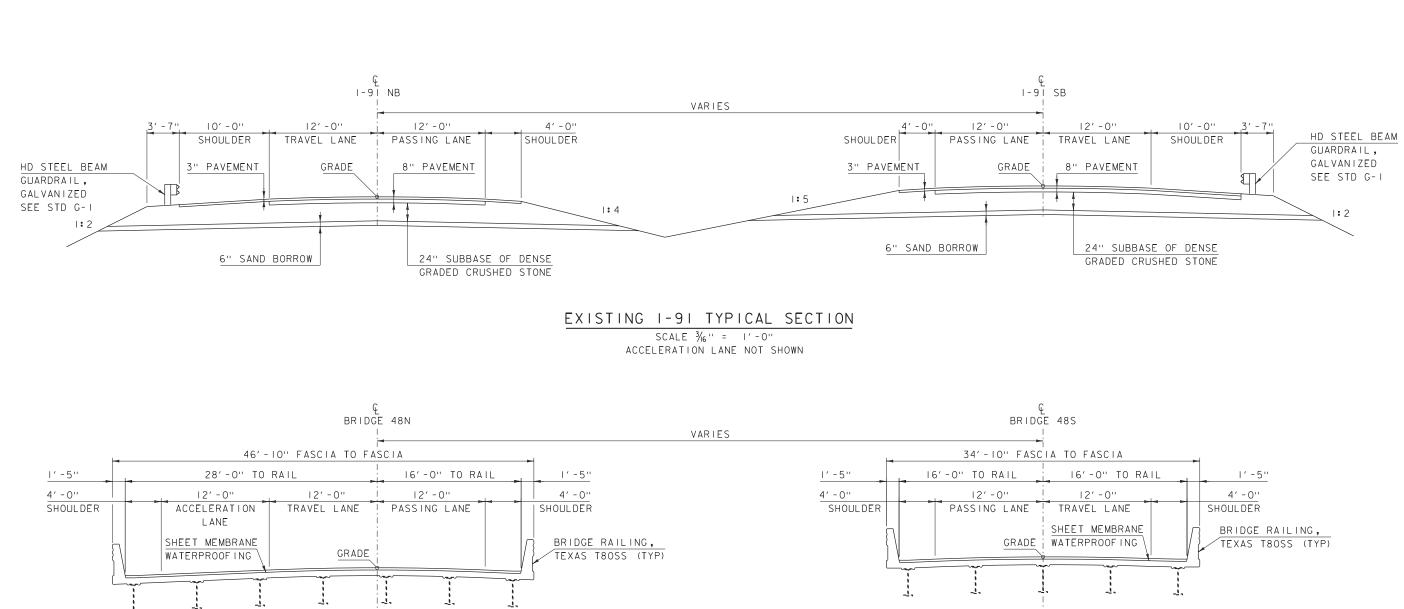


BRIDGE 48 N/S REHABILITATION TYPICAL SECTION

SCALE 3/16" = 1'-0" ALL DIMENSIONS ARE RADIAL UNLESS OTHERWISE NOTED

PROJECT NAME:	SPRINGEIEL D	
PROJECT NUMBER:	IM 091-1(83)	
FILE NAME: 12o574/ PROJECT LEADER: 1 DESIGNED BY: REHABILITATION TY	J.STONE	PLOT DATE: 15-MAY-2020 DRAWN BY: D.D.BEARD CHECKED BY: SHEET 22 OF 47

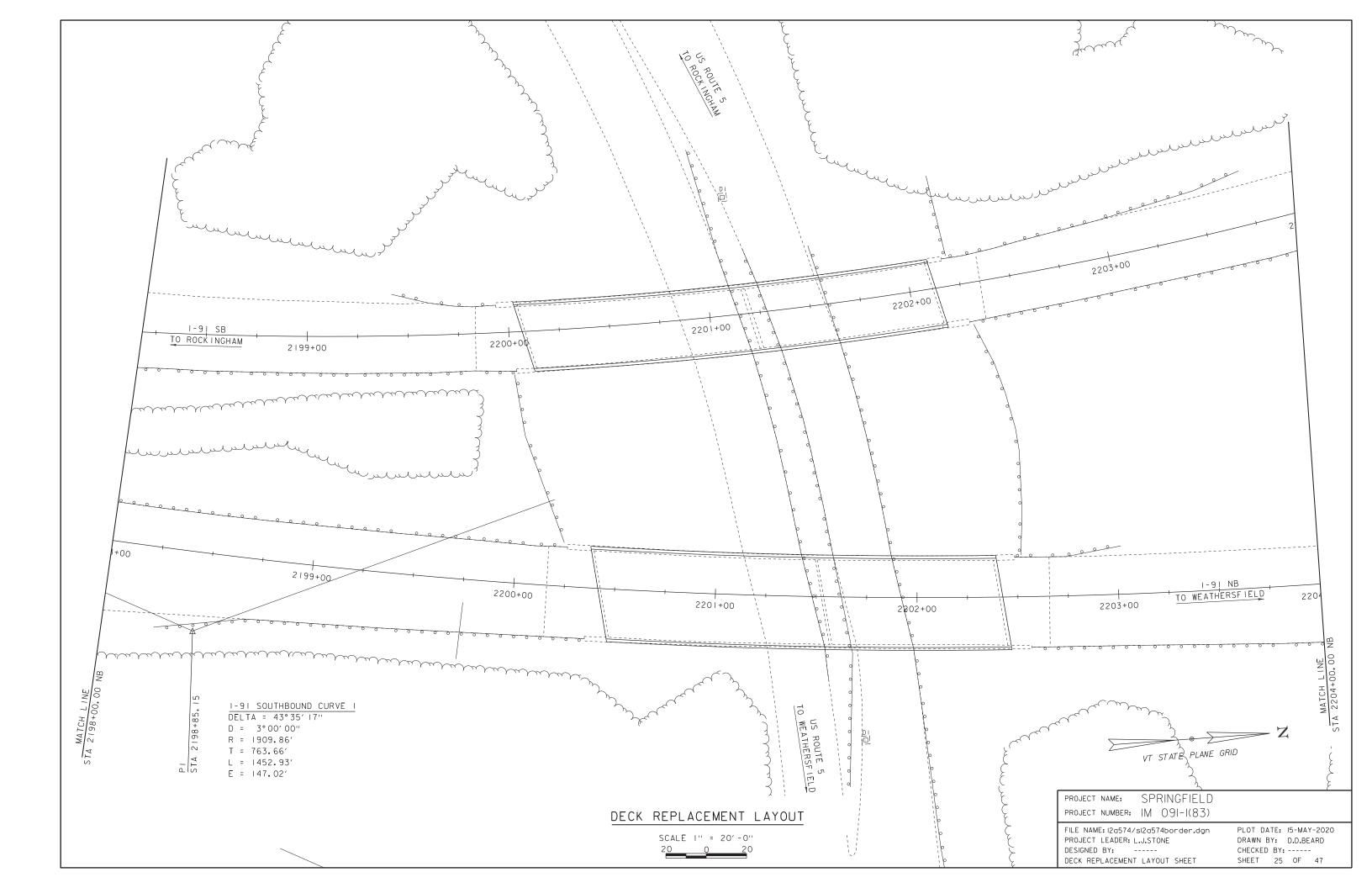


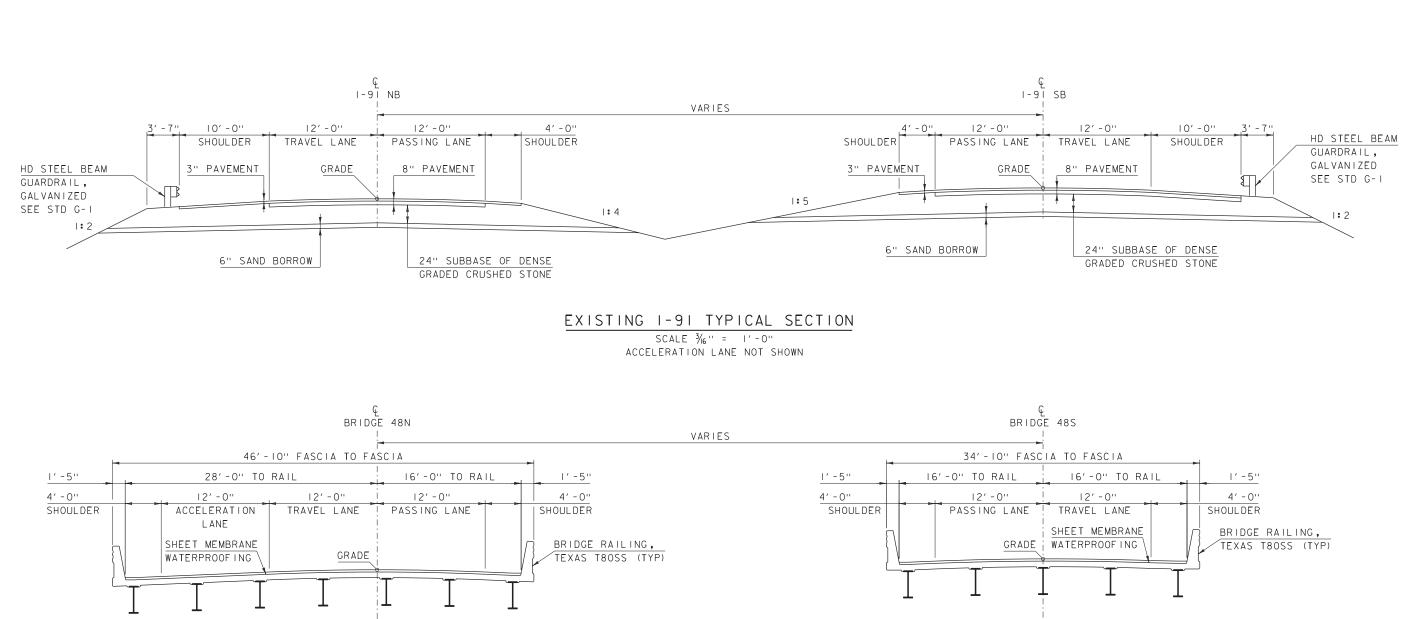


BRIDGE 48 N/S DECK REPLACEMENT TYPICAL SECTION

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PROJECT NAME:	SPRINGFIELD					
PROJECT NUMBER:	IM 091-1(83)					
FILE NAME: 12a574/	sl2a574typ.dgn	PLOT DATE: 15-MAY-2020				
PROJECT LEADER:	J.STONE	DRAWN BY: D.D.BEARD				
DESIGNED BY:		CHECKED BY:				
DECK REPLACEMENT	TYPICAL SECTIONS	SHEET 24 OF 47				

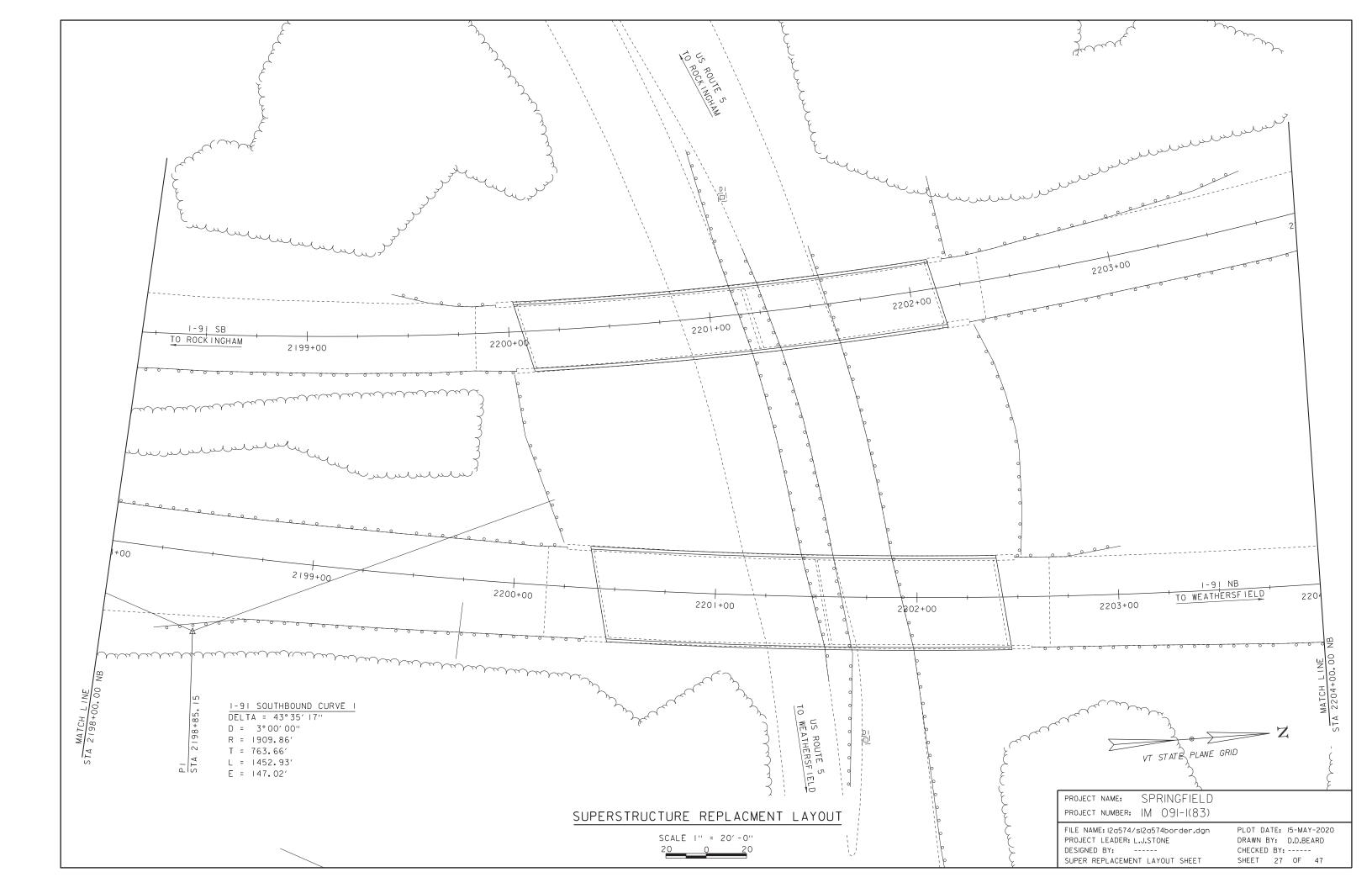


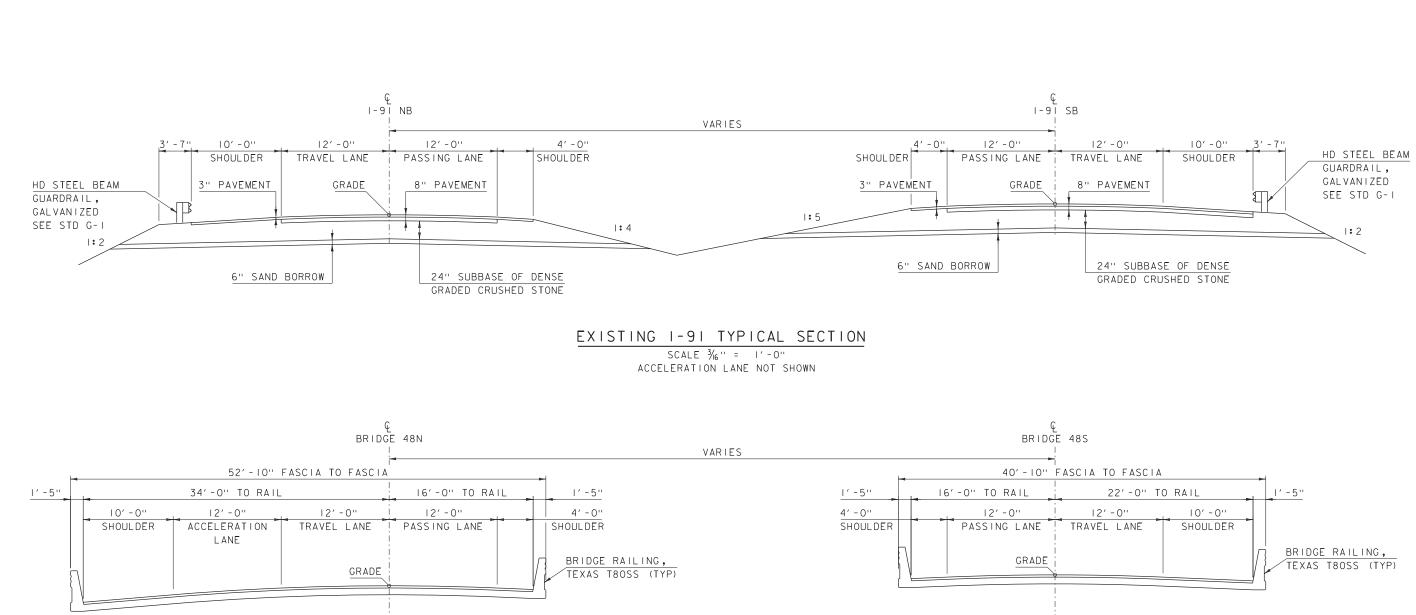


BRIDGE 48 N/S SUPERSTRUCTURE REPLACEMENT TYPICAL SECTION

SCALE 3/16 " = 1'-0" ALL DIMENSIONS ARE RADIAL UNLESS OTHERWISE NOTED

PROJECT NAME: PROJECT NUMBER:	SPRINGFIELD IM 091-1(83)	
FILE NAME: 12a574/s12a574+yp.dgn		PLOT DATE: 15-MAY-2020
PROJECT LEADER: L.J.STONE		DRAWN BY: D.D.BEARD
DESIGNED BY:		CHECKED BY:
SUPER REPLACEMENT TYPICAL SECTIONS		SHEET 26 OF 47

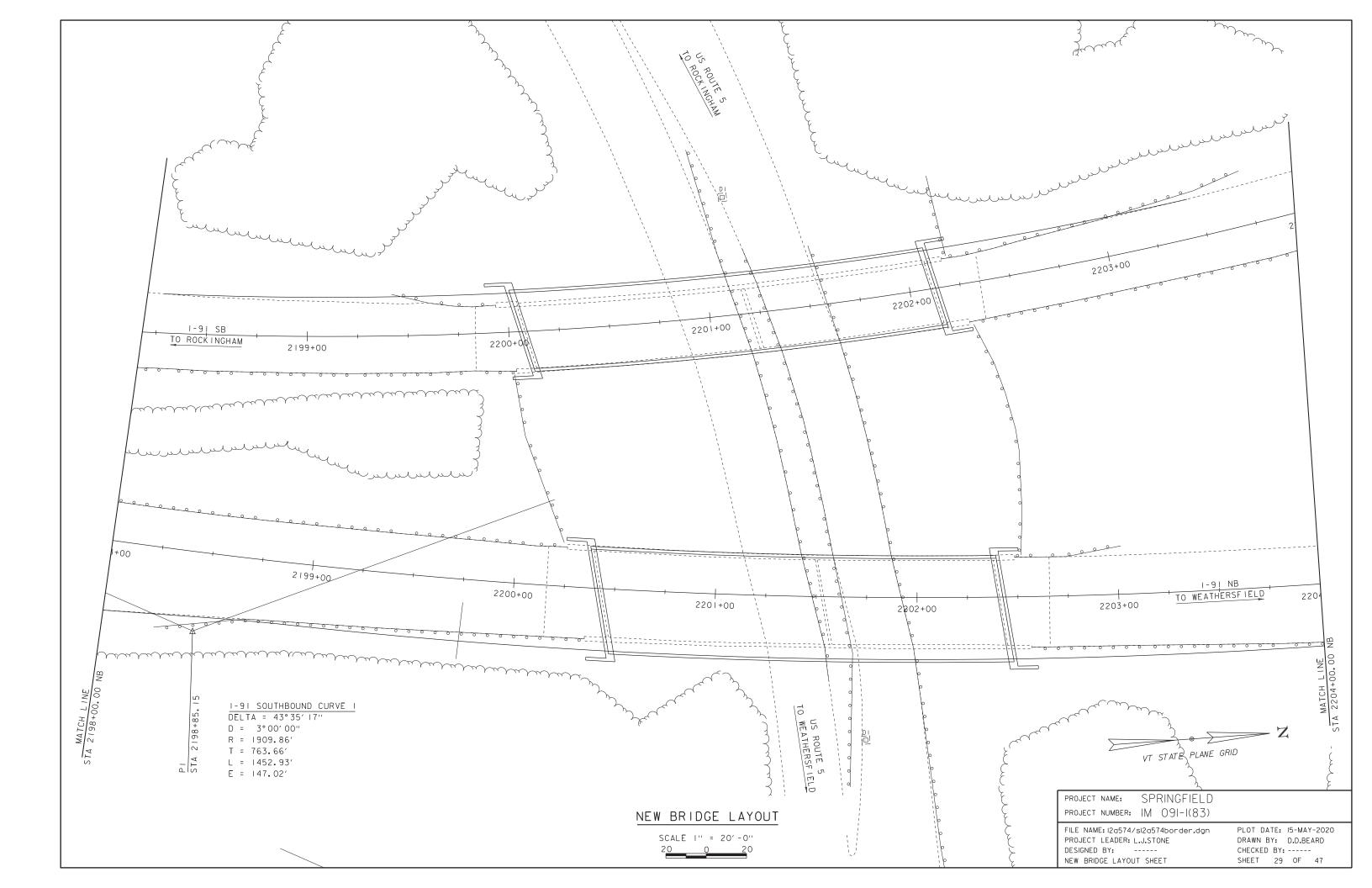


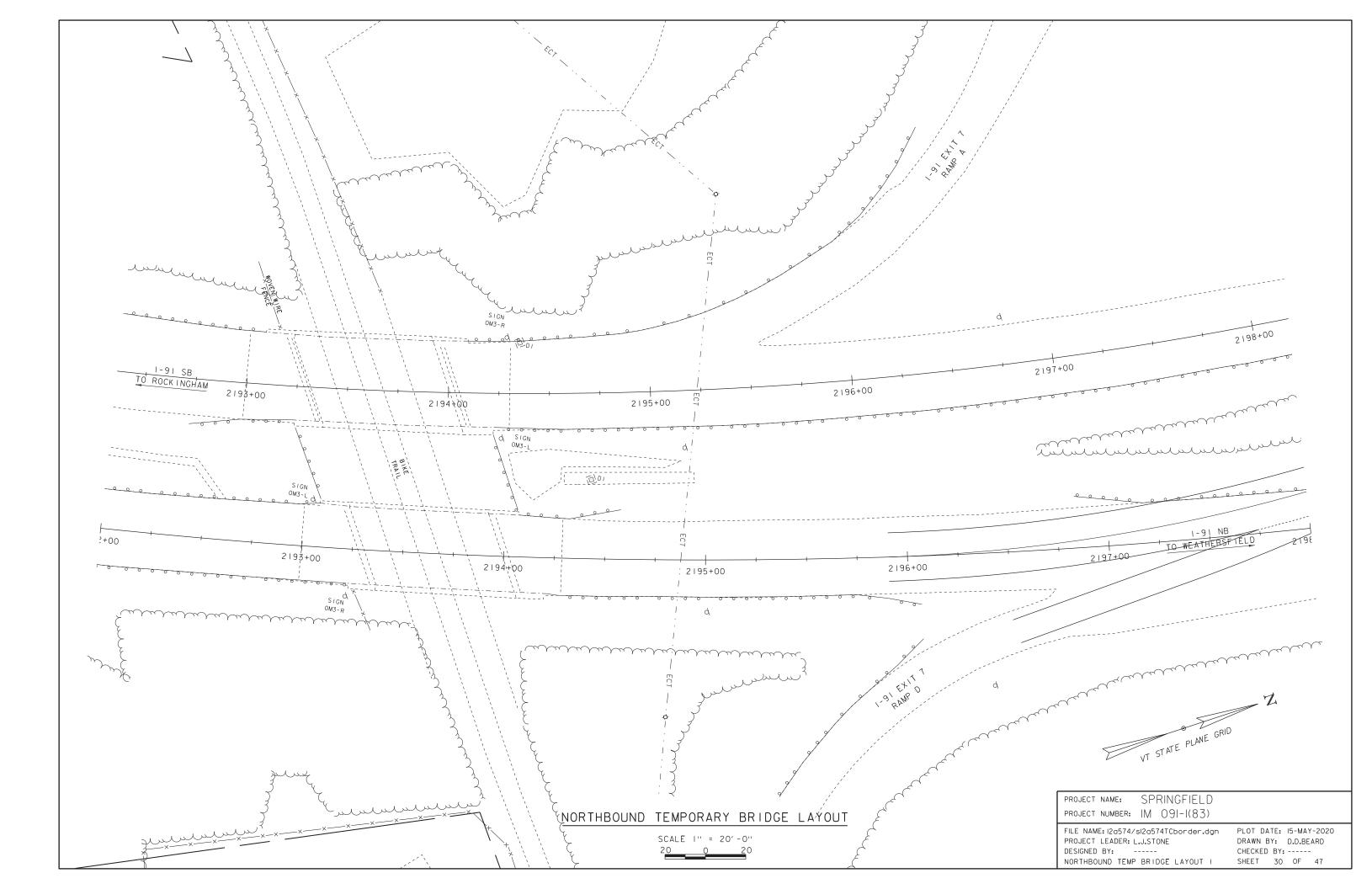


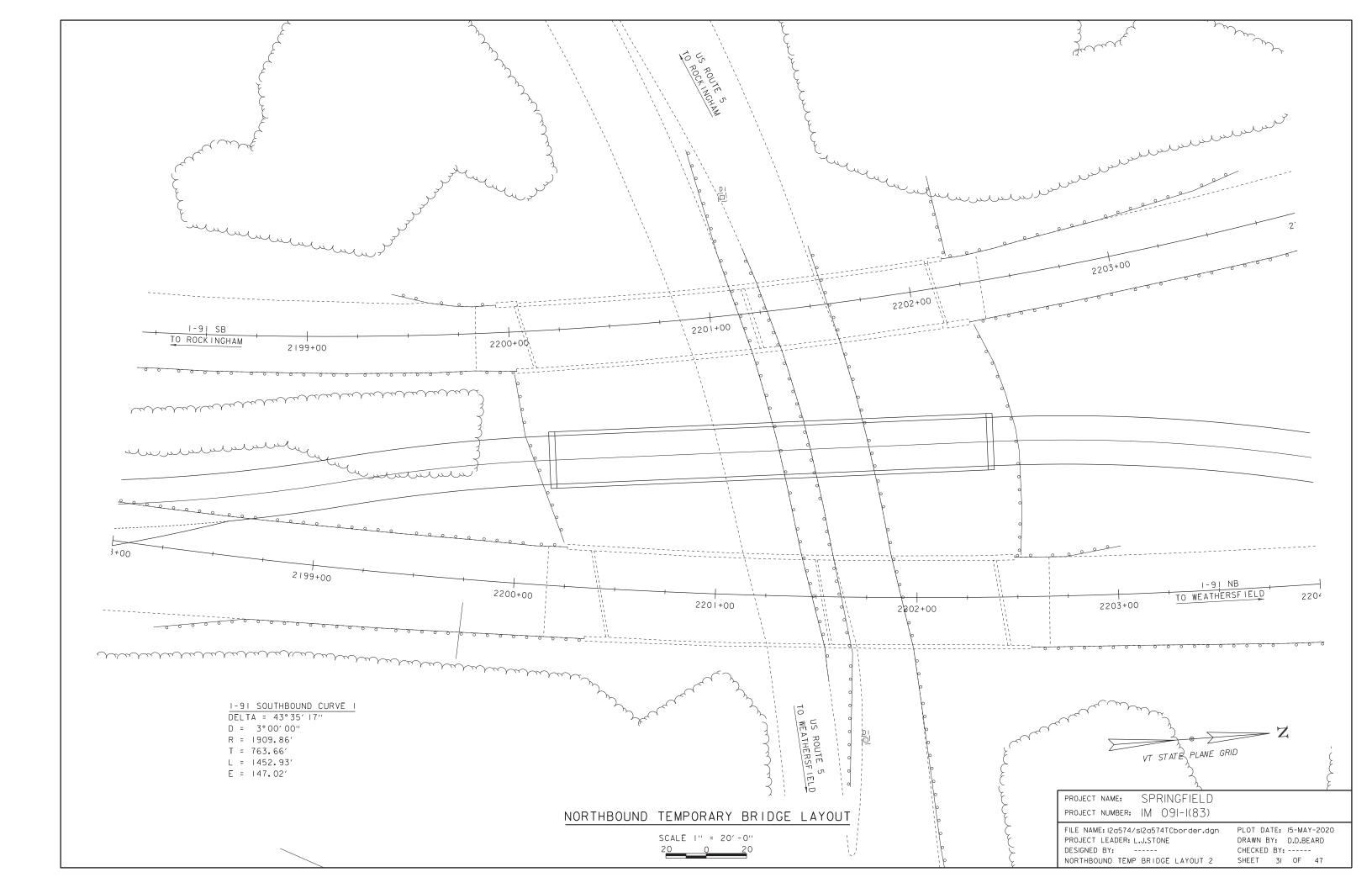
BRIDGE 48 N/S BRIDGE REPLACEMENT TYPICAL SECTION

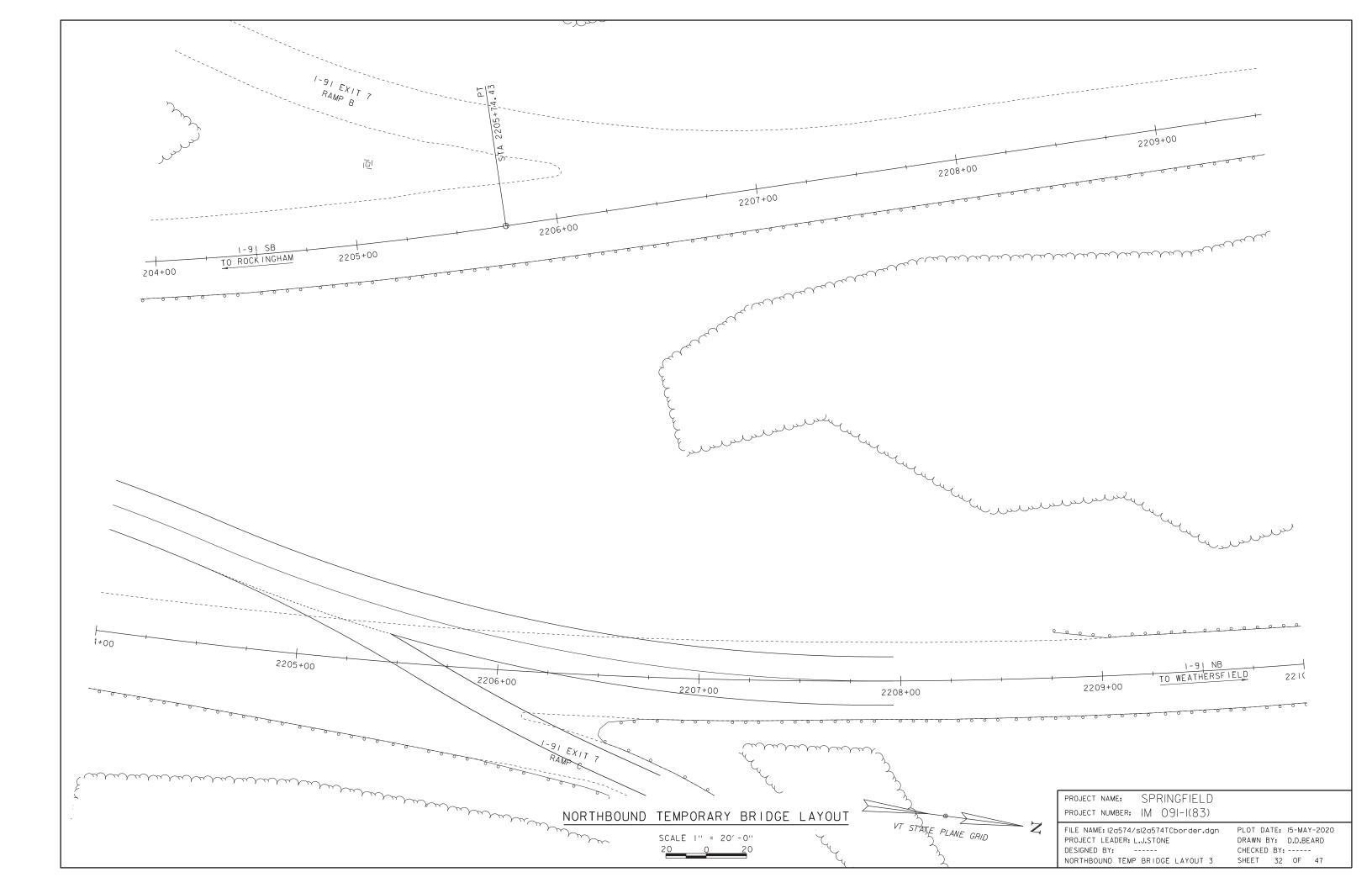
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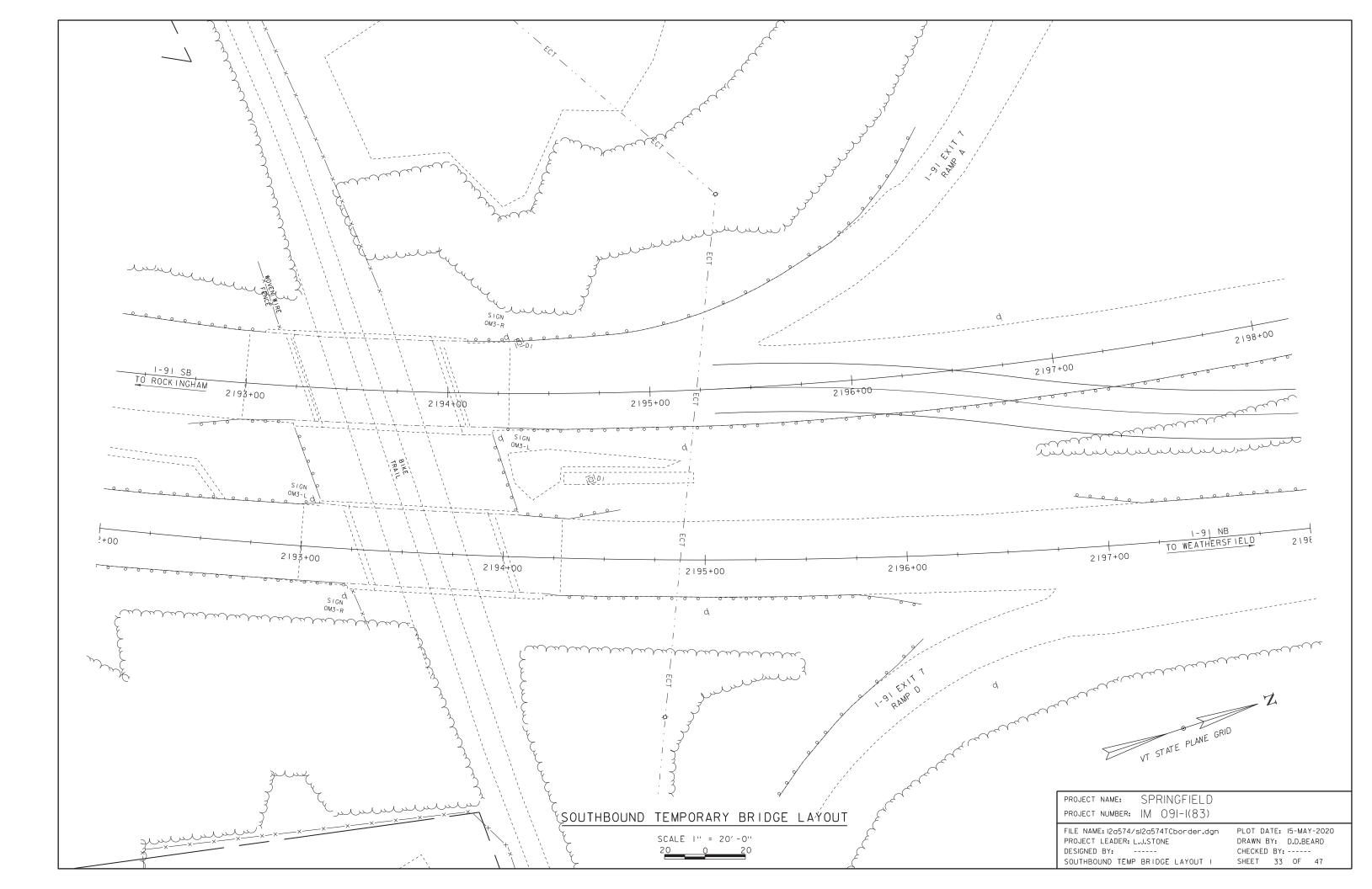
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project number: M 09 -1(83)	
FILE NAME: 12a574/s12a574typ.dgn PROJECT LEADER: L.J.STONE DESIGNED BY: BRIDGE REPLACEMENT TYPICAL SECTIONS	PLOT DATE: 15-MAY-2020 DRAWN BY: D.D.BEARD CHECKED BY: SHEET 28 OF 47

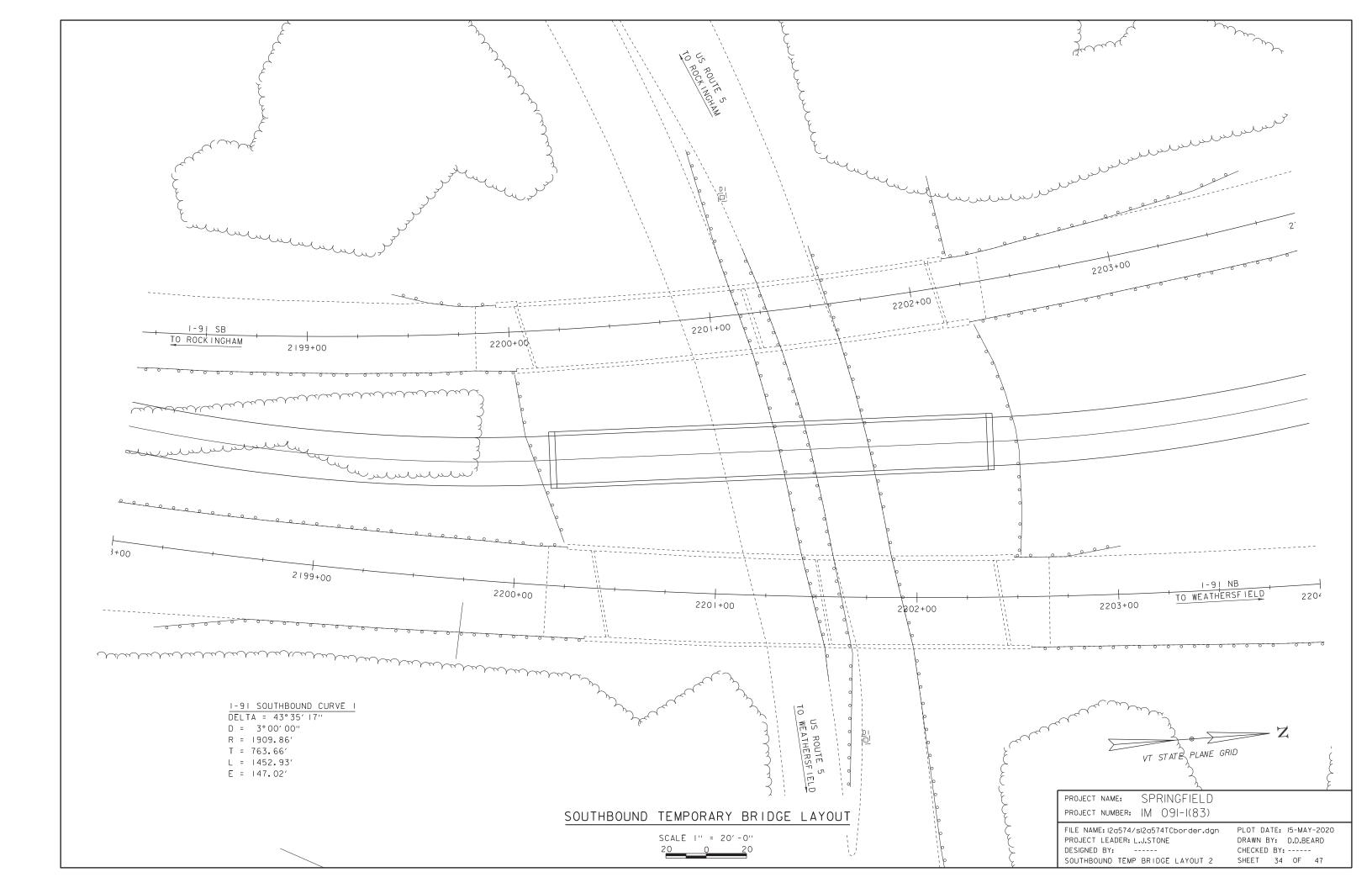


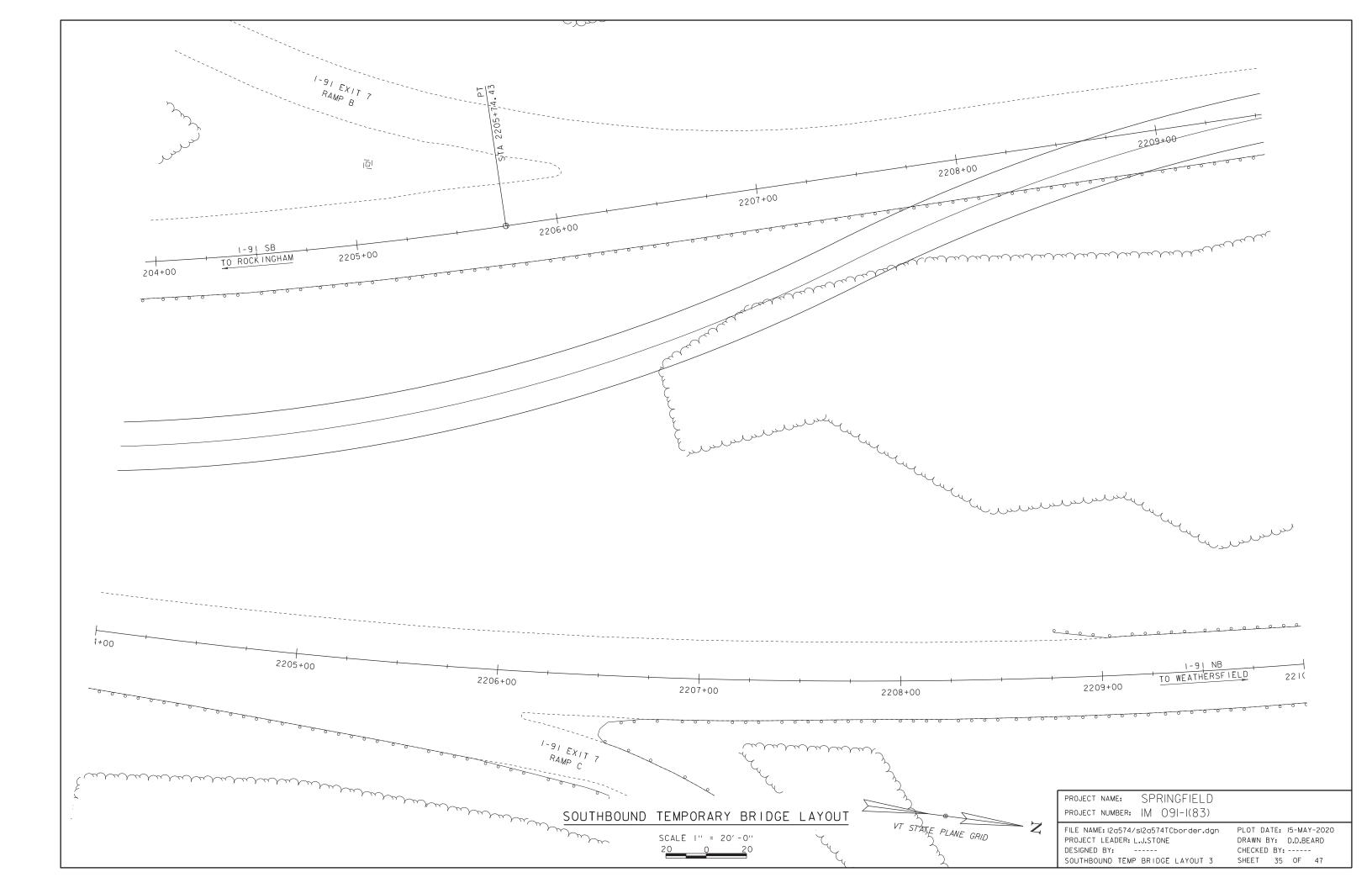


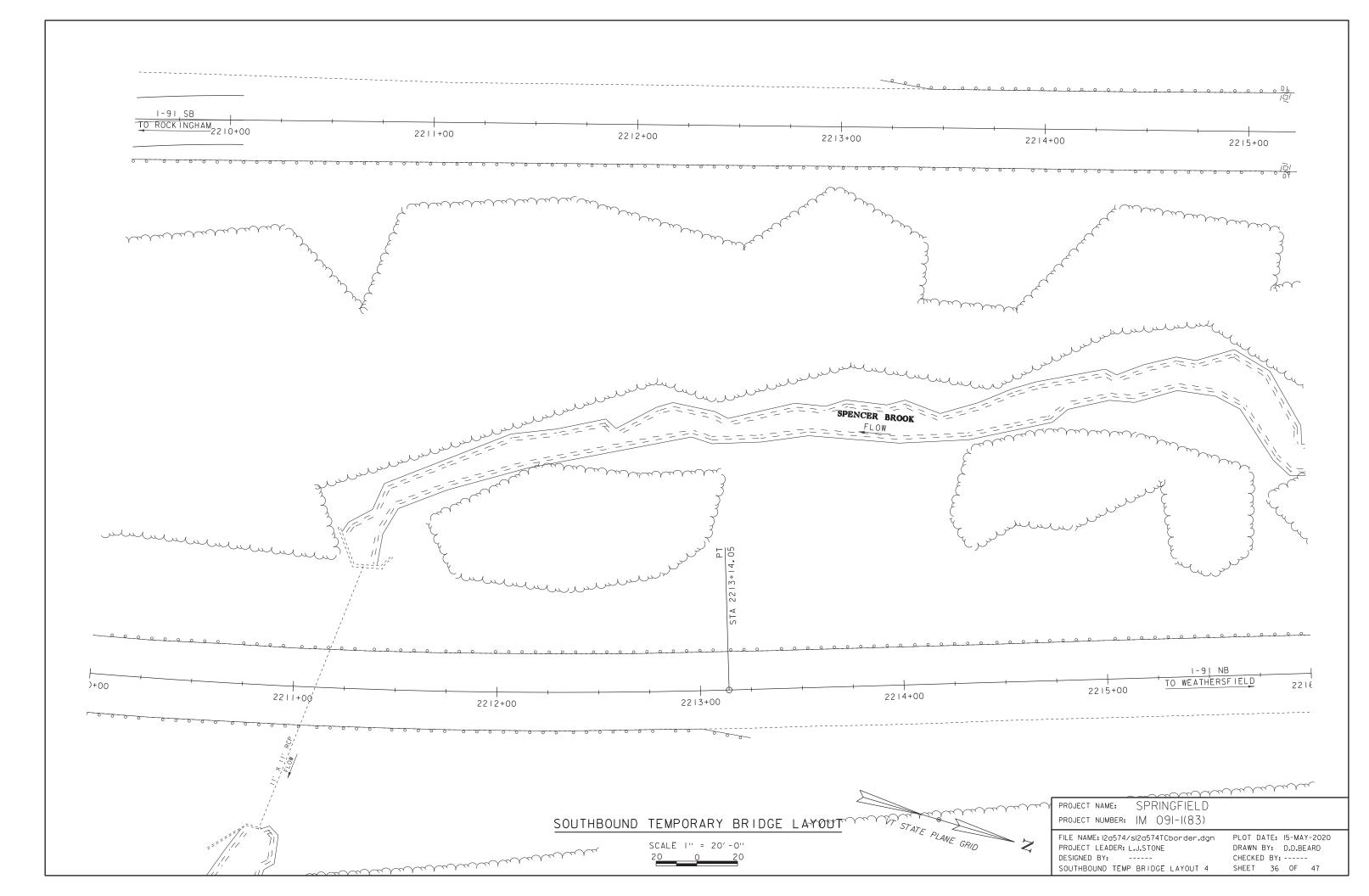


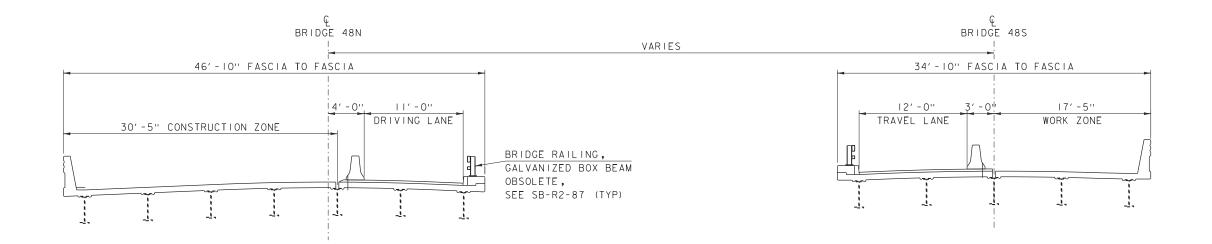






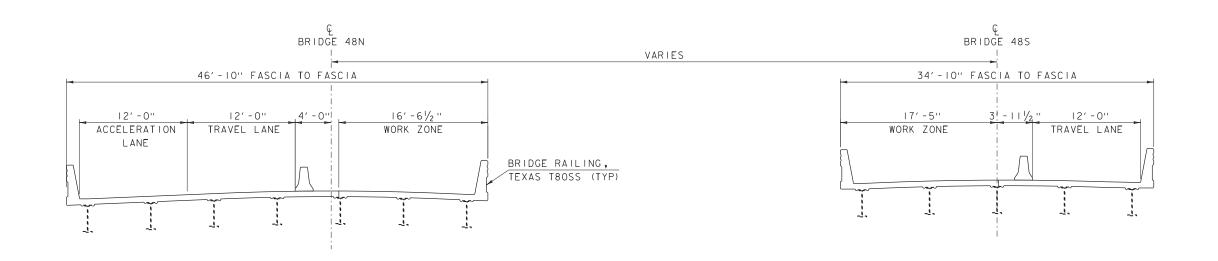






BRIDGE 48 N/S PHASE I TYPICAL SECTION

SCALE $\frac{3}{16}$ " = 1'-0" All DIMENSIONS ARE RADIAL UNLESS OTHERWISE NOTED



BRIDGE 48 N/S PHASE 2 TYPICAL SECTION

SCALE ¾" = I'-O" ALL DIMENSIONS ARE RADIAL UNLESS OTHERWISE NOTED

PROJECT NAME:	SPRINGFIELD	
PROJECT NUMBER:	IM 091-1(83)	
FILE NAME: 12o574/ PROJECT LEADER: 1 DESIGNED BY: PHASING TYPICAL S		PLOT DATE: 15-MAY-2020 DRAWN BY: D.D.BEARD CHECKED BY: SHEET 37 OF 47

